

# PSPICE Simulation of Crosstalk on GEM Strips

M. Hohlmann

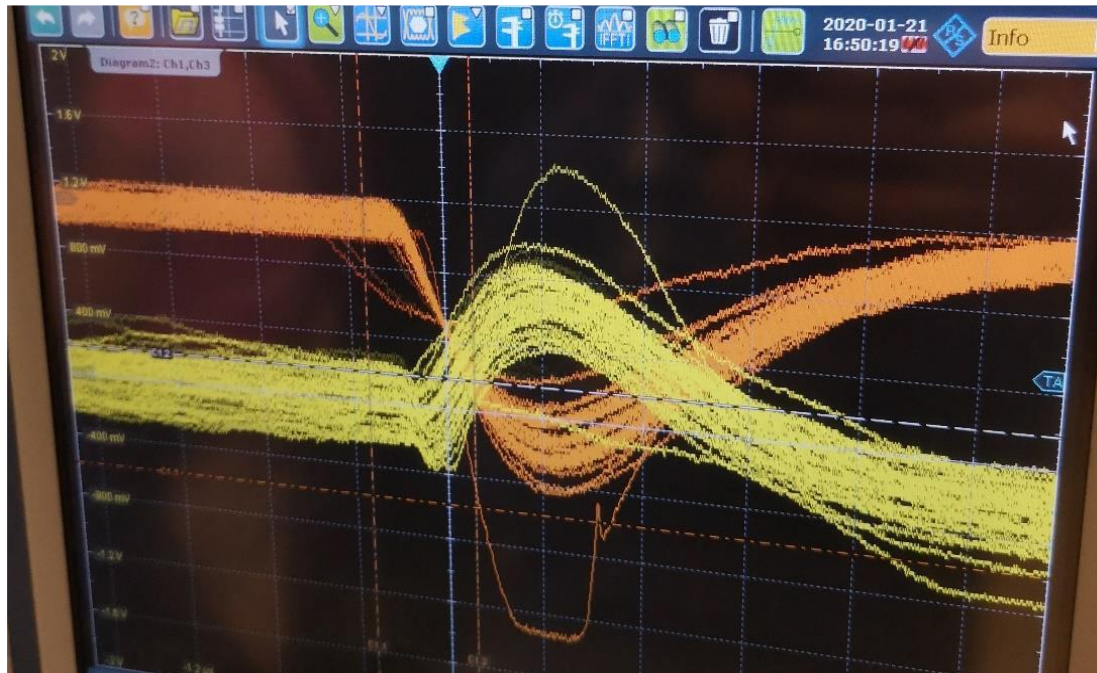
FIT

5/19/2020

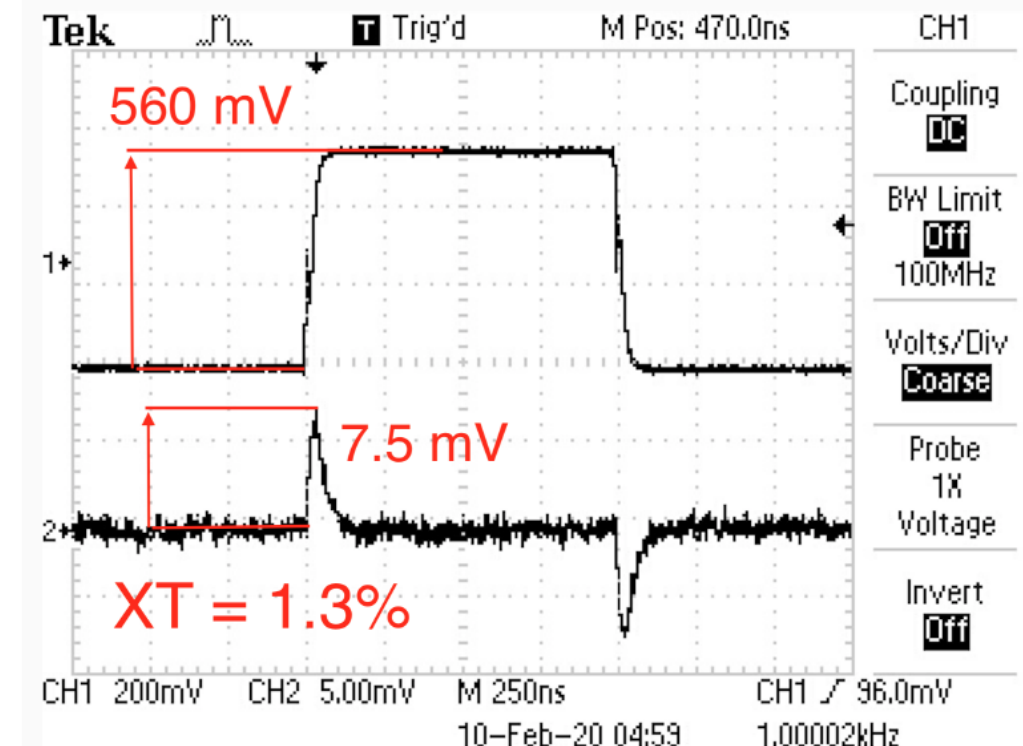
GEM Phase 2 Upgrade Workshop – May 2020

# Motivation

Understand the difference in **observed polarity of crosstalk (XT) pulses** measured in tests with **normal GEM avalanche mode** at CERN and tests with **injecting voltage pulses** into readout strips at FIT.



Davide Fiorina's measurements on 10x10 GEM:  
**opposite sign** of signal and XT



Stephen Butalla's measurement with pulser:  
**same sign** of signal (on leading edge) and XT

# Motivation cont'd

- Why is XT only observed in **double**-segmented foils (GE2/1, ME0) and not in single-segmented foils (GE1/1) ?
- Achieve a better understanding of the XT, so **XT mitigation strategies** can be developed.

⇒ **Built an independent detailed SPICE model of GEM detector for testing**

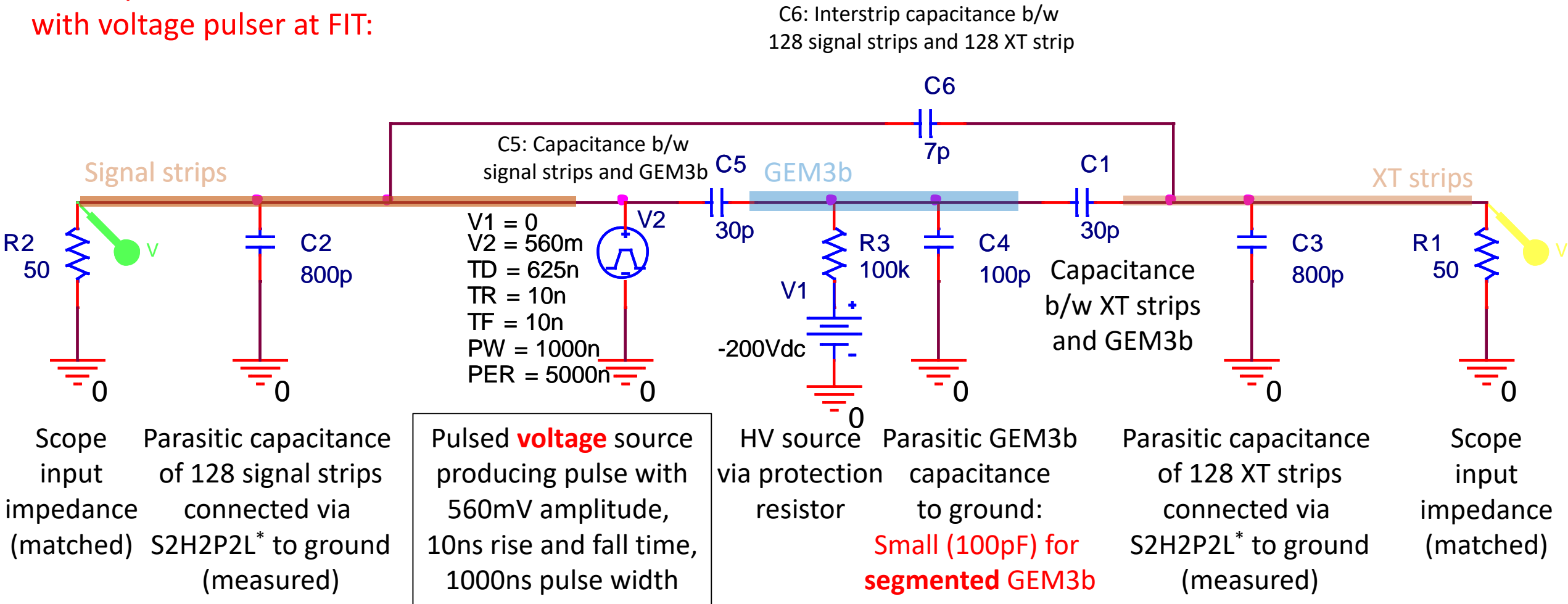
- Use the `cadence` / ORCAD PSPICE suite for modelling

# PSPICE Model 1

Voltage pulser measurements

# 1. Model Circuit for pulser measurements

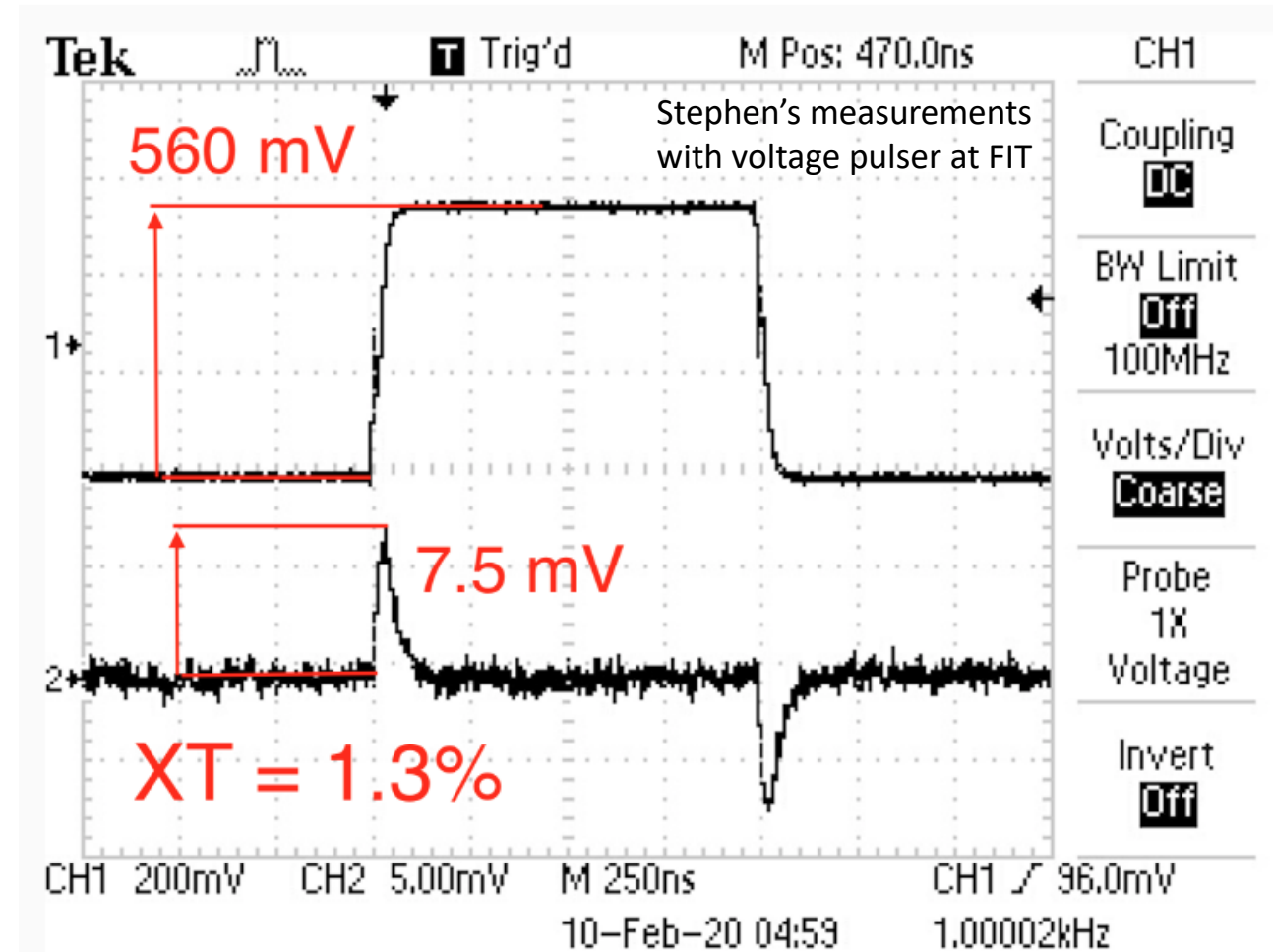
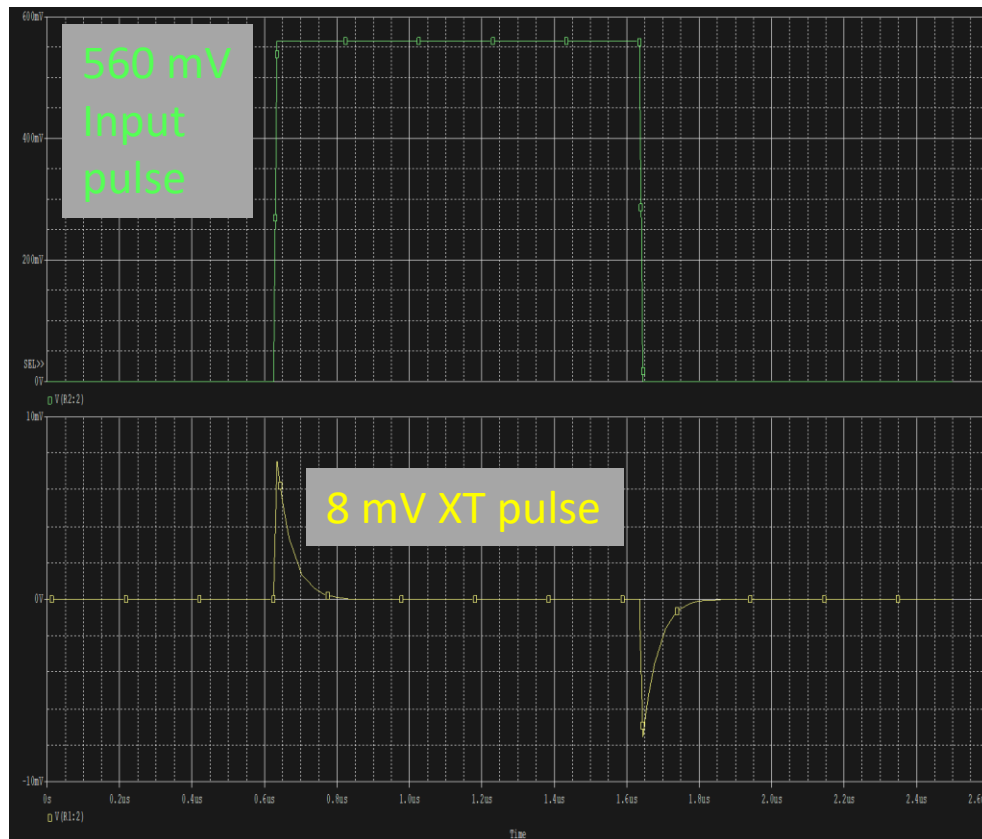
For Stephen's measurements  
with voltage pulser at FIT:



\* "Strip to Hirose to Panasonic to LEMO" adapter

# 1. Pulse simulation vs. measurement

Simulation output:



## Main observations:

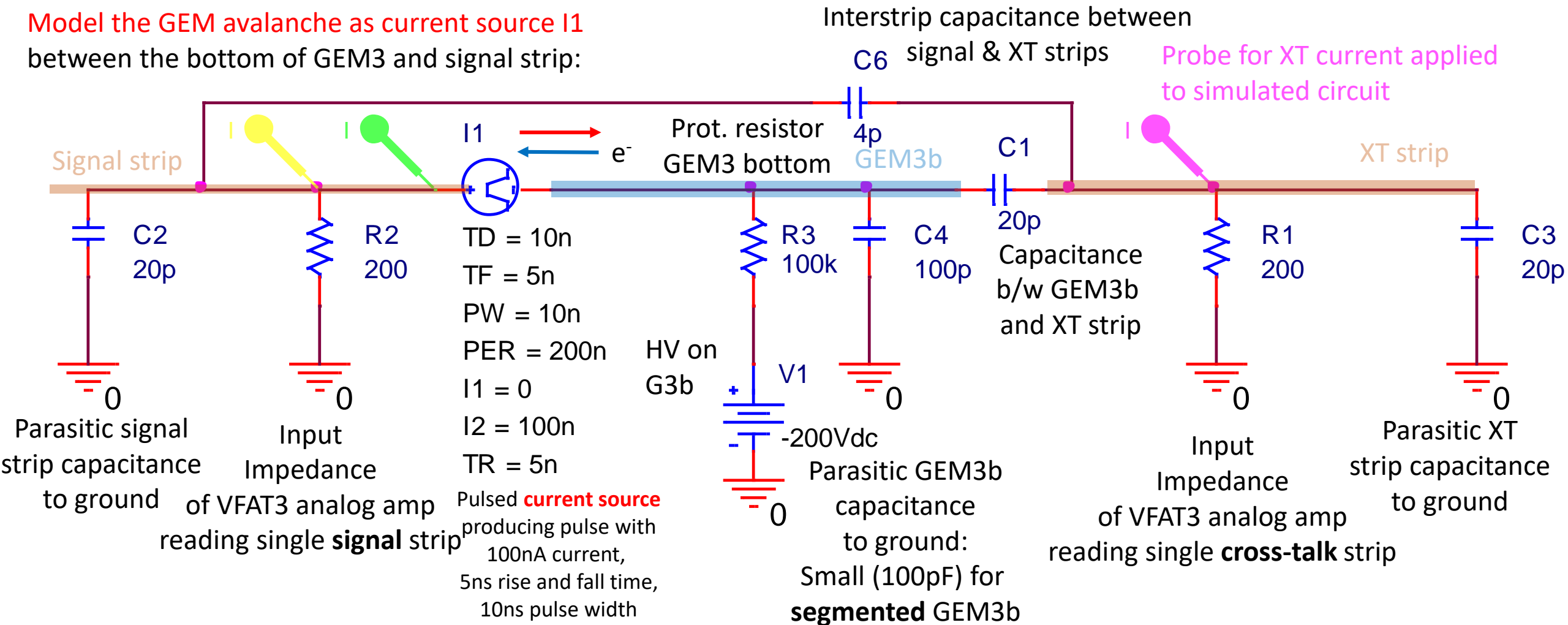
- Simulation and measurement **agree** with respect to cross-talk (XT) polarity, amplitude, and RC time constant !
- This implies that the cross talk pulse is indeed **due to capacitive coupling**
- Input voltage pulse and XT voltage pulse **have THE SAME POLARITY on leading edge**

# PSPICE Model 2

Normal GEM operation with GEM avalanches, e.g. with  $\alpha$ -source

# 2. PSPICE circuit implementation for gas avalanche

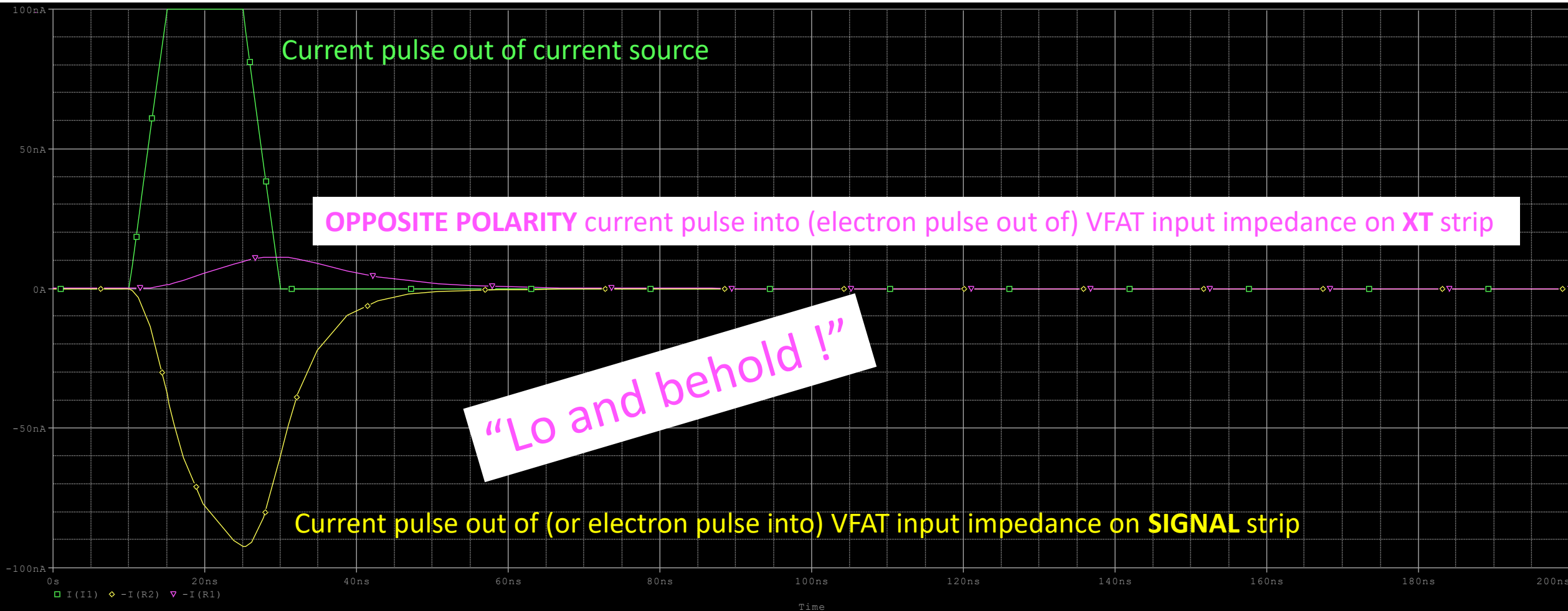
Model the GEM avalanche as current source I1 between the bottom of GEM3 and signal strip:



Current source: 10,000 primary electrons (1.6 fC) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$   
(note that this doesn't even take gas gain into account)



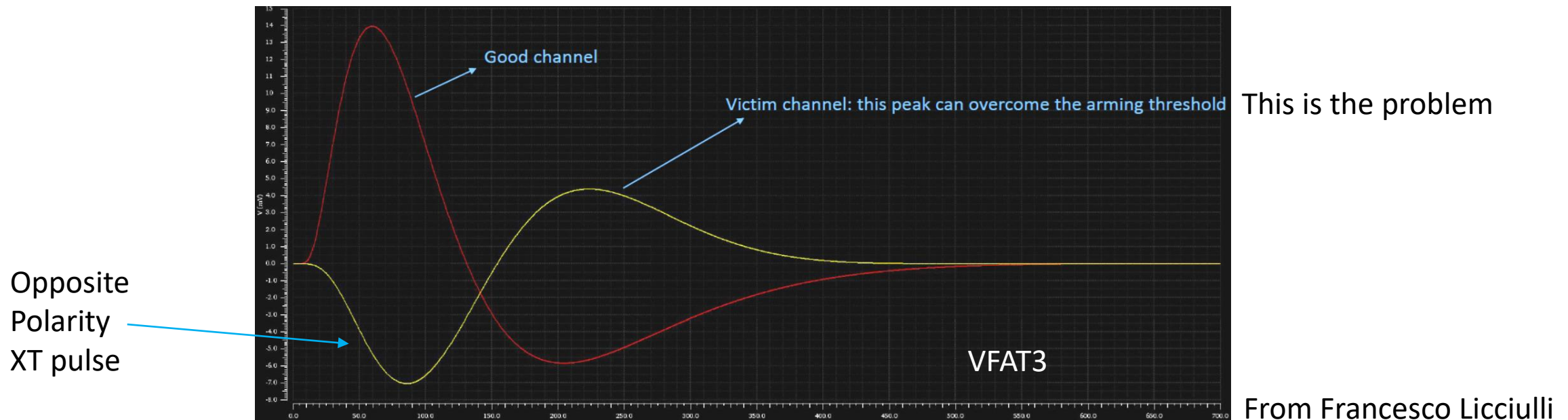
# 2. Pulse analysis for gas avalanche



**Main observation:** The electron pulse into the VFAT amp connected to the **signal strip** (yellow) and the electron pulse into the VFAT amp connected to the **XT strip** (purple) now have **OPPOSITE polarity!** This is different from the result with the pulser where we have same polarity.

# Impact on VFAT3

- The opposite-polarity pulse on the XT strip, i.e. at the **input** of the VFAT3 analog amplifier, produces also an opposite-polarity XT signal at the **output** of the VFAT3 analog amplifier and as such would be harmless.
- However, due to the shaping that occurs in the VFAT3 analog amplifier, the XT signal has an overshoot after some 200ns that goes in the *same* direction as the leading pulse on the signal strip:

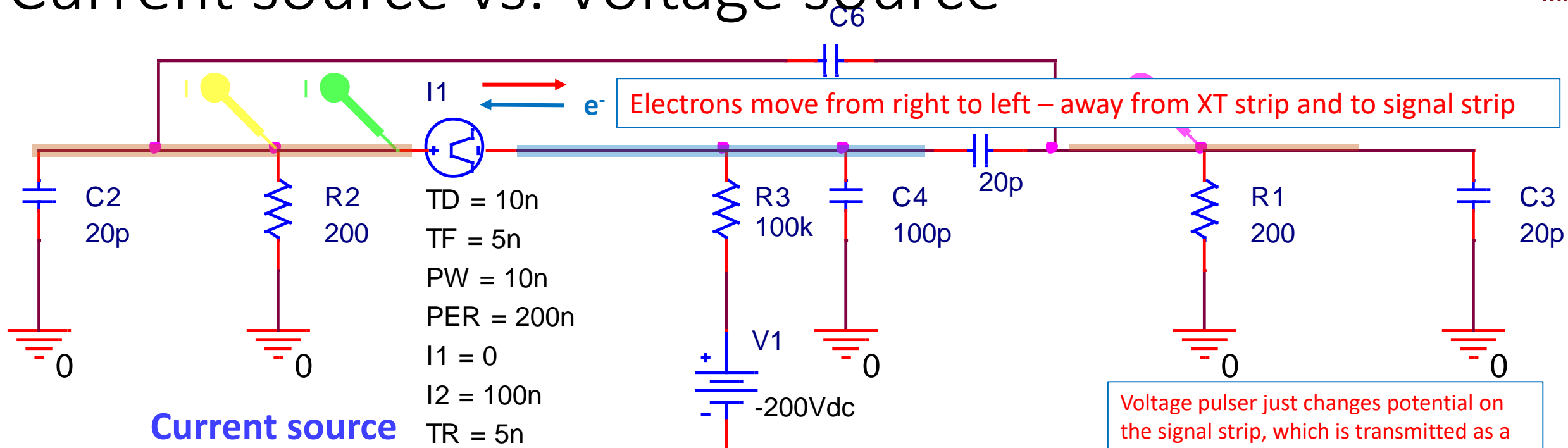


# Making sense of results

From the two models we now finally understand why we get **opposite polarity** between a good signal pulse and a XT pulse at the VFAT input (and hence output) when we have a *gas avalanche* in the GEM ( $\alpha$ -source) as opposed to **the same polarity** between a good signal pulse and a XT pulse at the VFAT input & output when we pulse the readout strips with a *voltage pulse*:

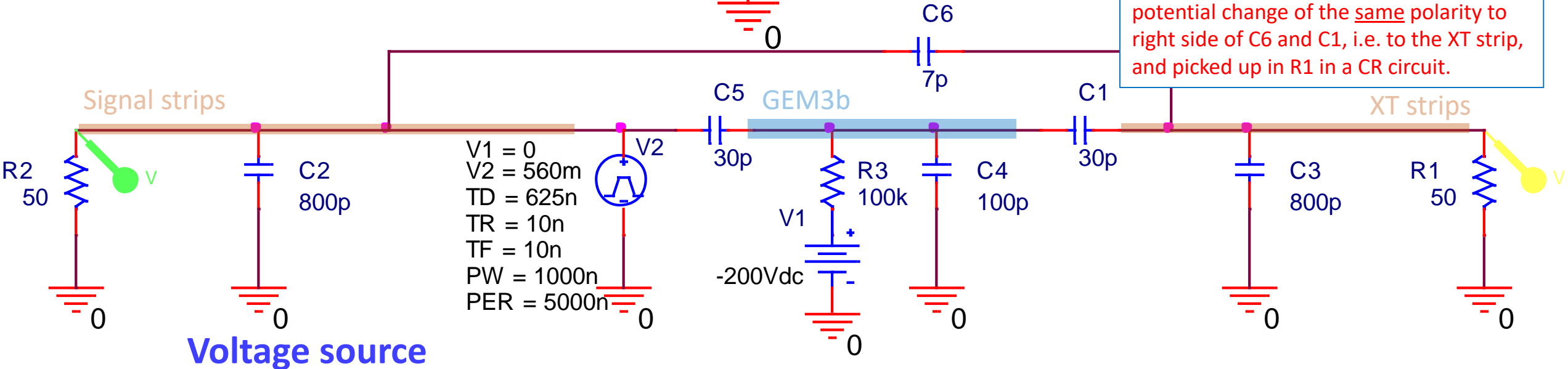
=> *“Current sources and voltage sources are not the same thing!”*

# Current source vs. Voltage source



**Current source**

Voltage pulser just changes potential on the signal strip, which is transmitted as a potential change of the same polarity to right side of C6 and C1, i.e. to the XT strip, and picked up in R1 in a CR circuit.



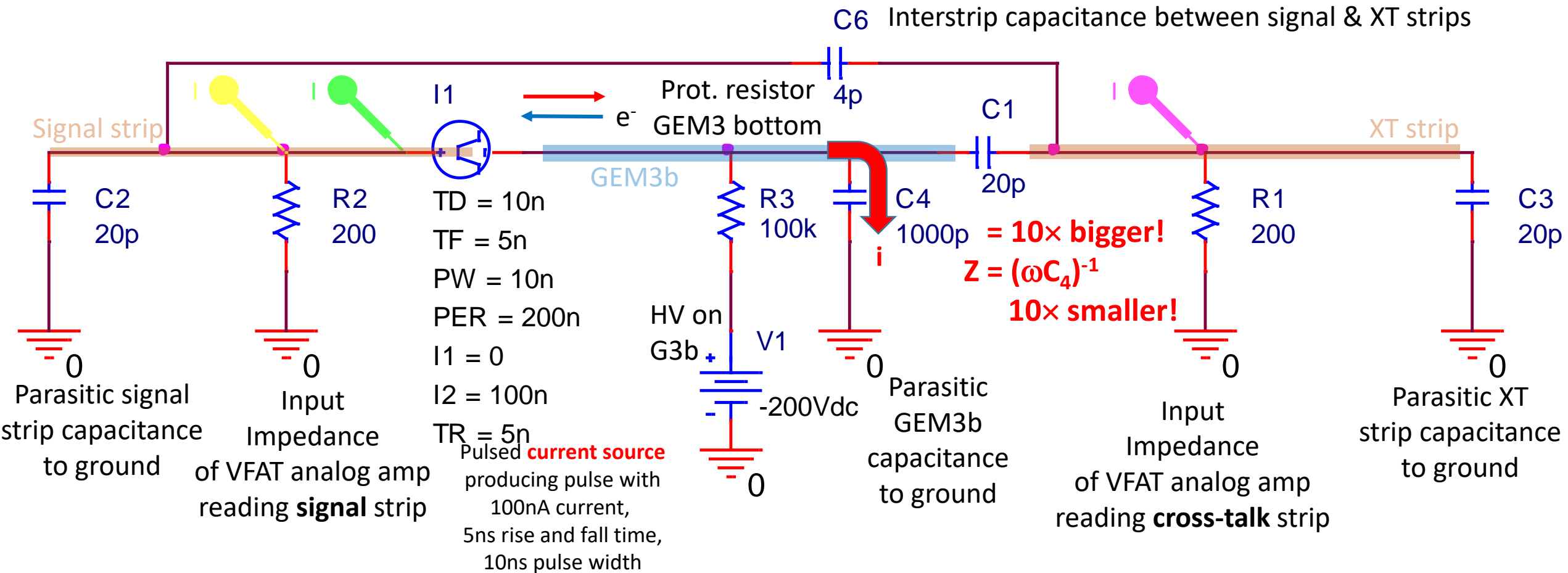
**Voltage source**

# Making sense of experimental observations

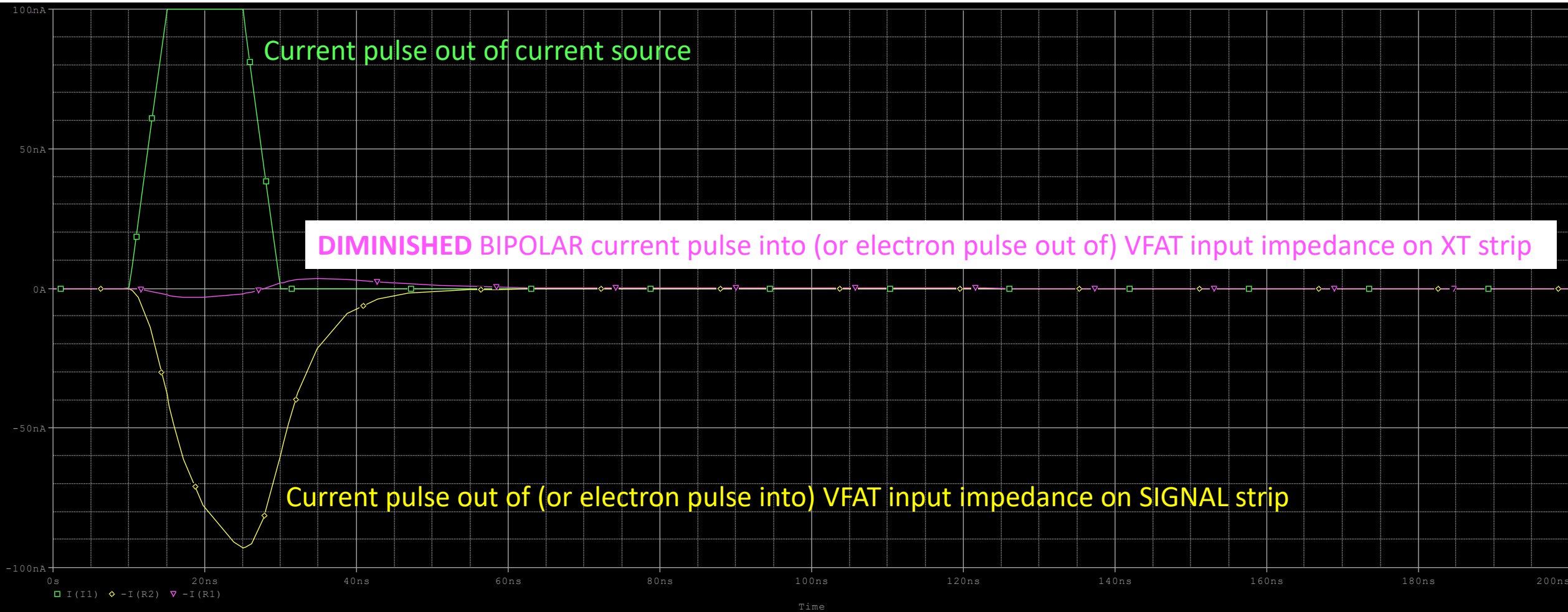
- We have only seen the XT in **double-segmented foils** where GEM3b HV segments are connected to HV via 100 k $\Omega$  protection resistors.
- We have NOT seen the XT in single-segmented foils (GE1/1) where the single GEM3b HV segment is **connected to HV without a protection resistor**. (Only the other foil side GEM3t is protected with 10 M $\Omega$  resistors).

# 3. Increased GEM3b capacitance to GRD

- In this circuit, the increased capacitance of GEM3 bottom provides a **much reduced impedance Z for sinking the current from the current source to ground.**
- As a consequence, the amount of **XT current** that can flow into C1 is reduced.
- **This explains why XT is observed on double-segmented foils, but not on single-segmented foils!**



# 3. Increased GEM3b capacitance to GRD



**Main observation: The XT pulse is DIMINISHED by a factor  $\approx 4$  and becomes bipolar!**

# Mitigation strategies: Increase GEM3b cap.

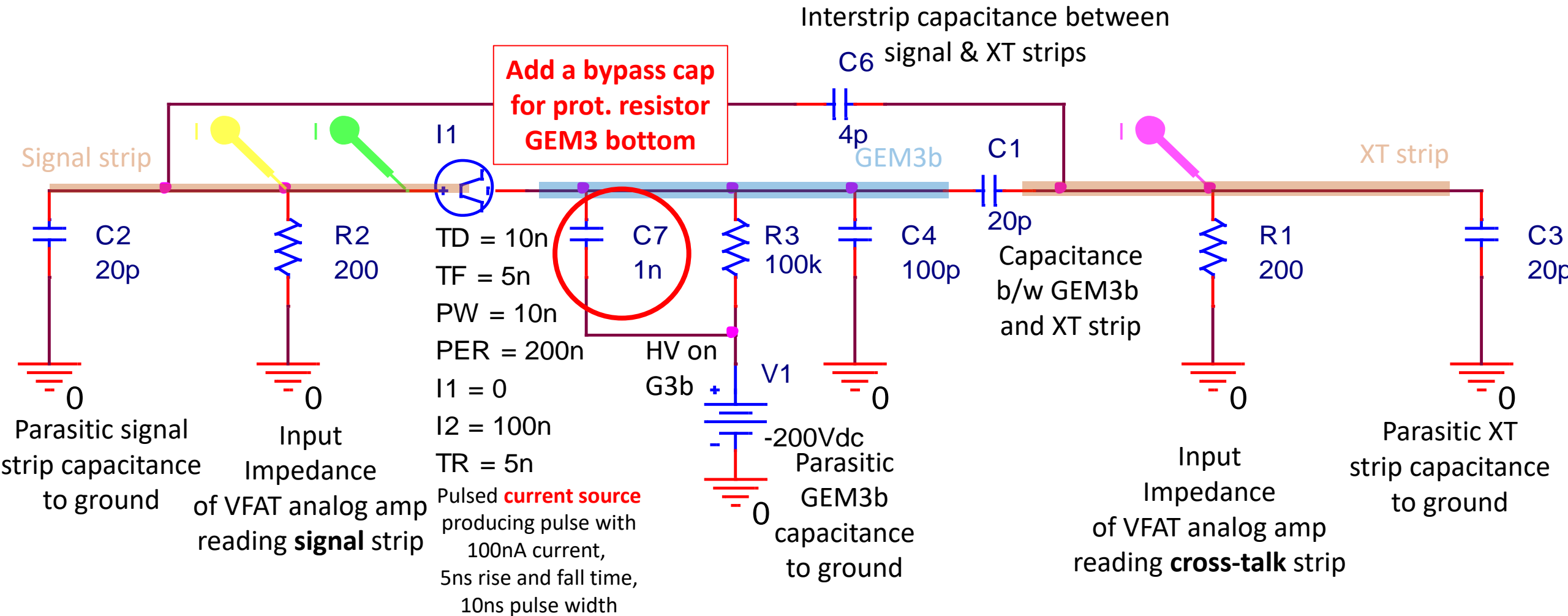
- Ok, that works! It is also confirmed by the tests at CERN where  **$\approx 10$  HV segments are connected back together** on GEM3b to increase their capacitance should show a reduction in XT (see Jeremie's and Stephen's talks).
- Note that the SIGNAL current is barely affected because the current source directly pumps electrons into the attached VFAT3 input.
- That is of course a good thing because we do not want to compromise the actual signal when mitigating the crosstalk.
- **Caveat:** Increasing foil capacitance will diminish discharge mitigation!



# Mitigation strategies: Bypass Capacitor

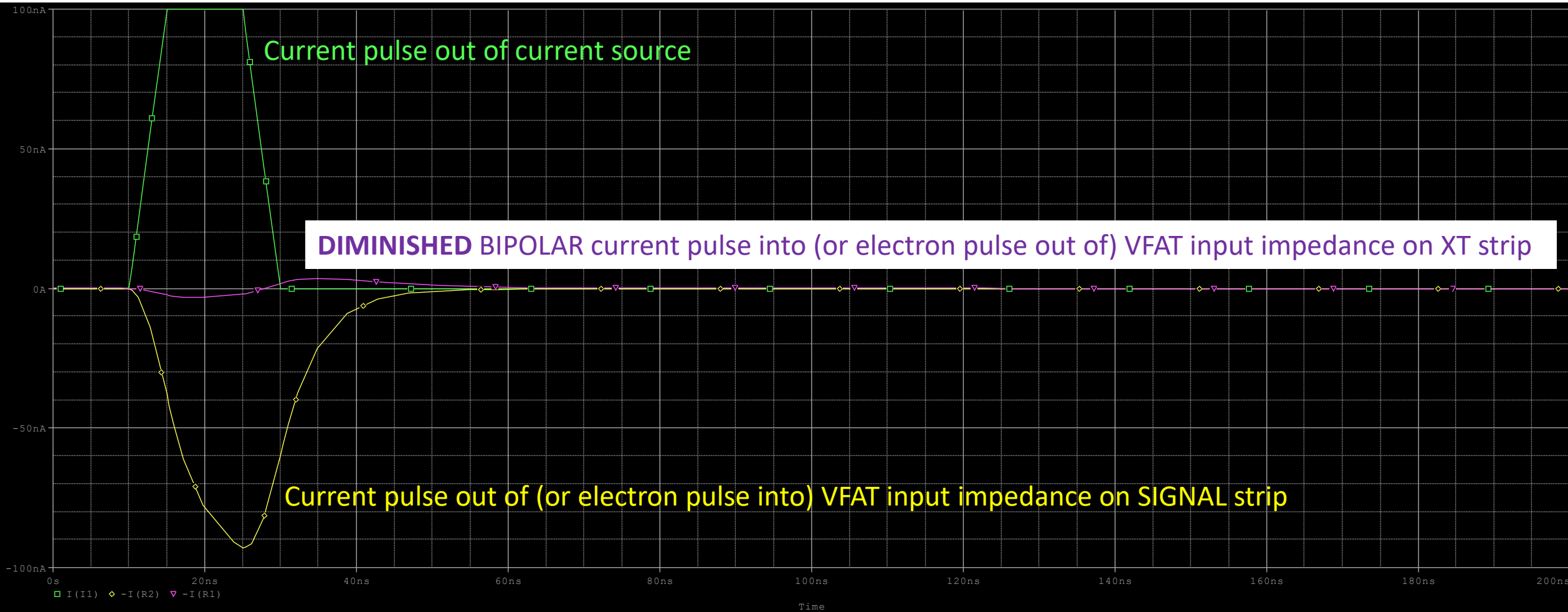
- Another strategy that has been suggested is to put a **bypass capacitor around the protection resistor** that will provide an additional path to ground for the AC current from GEM3b (but not for DC, i.e. HV)
- This will also decrease GEM3b impedance to ground
- Let's place such a capacitor with  $C_7 = 1000\text{pF} = 1\text{nF}$

# 4. Place a bypass cap. on 100k protection resistor



Current source: 10,000 primary electrons (1.6 fC) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$   
 (note that this doesn't even take gas gain into account)

# 4. Place a 1 nF bypass cap. on 100k protection resistor



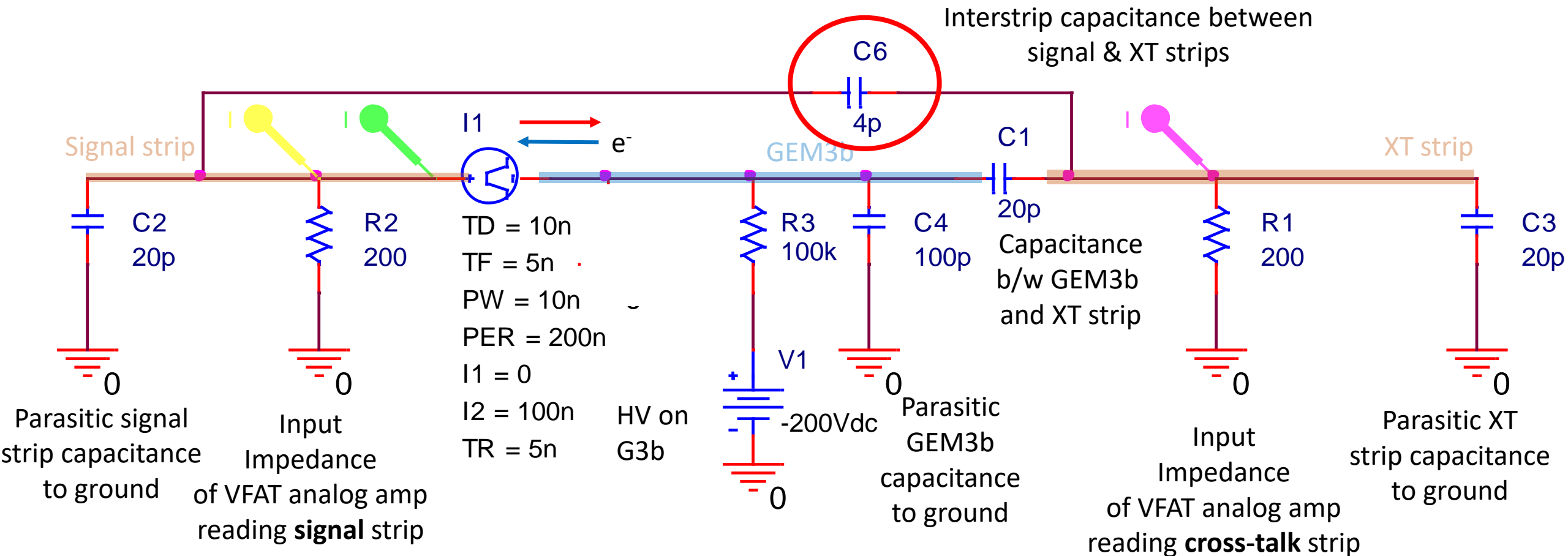
**Main observation: The XT pulse is DIMINISHED by a factor  $\approx 4$  and becomes bipolar!**

# Mitigation w/ bypass capacitor

- Ok, that works, too! This was also confirmed experimentally in Stephen's tests at FIT – see previous talk.
- However, this approach ultimately requires adding a cap to *each* HV segment on the foil because that is where the 100k protection resistors are located.
- This might be tricky to implement and the **bypass capacitors must be very HV stable in the long run.**
- *Probably not our best choice.*

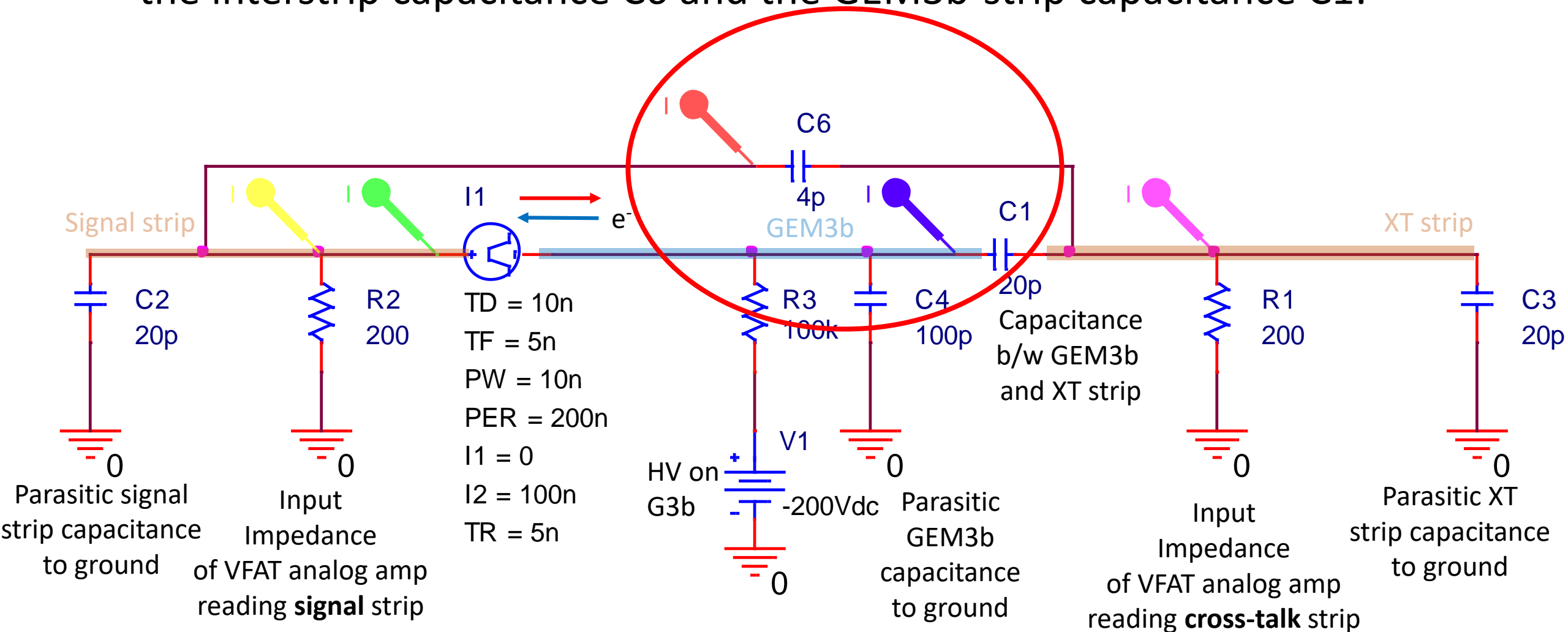
# Mitigation strategies: Limitations

- Larger capacitance on GEM3b and bypass capacitors can *reduce* crosstalk, **but not fully eliminate** it because there is still XT current through C6 due to the **interstrip** capacitance.

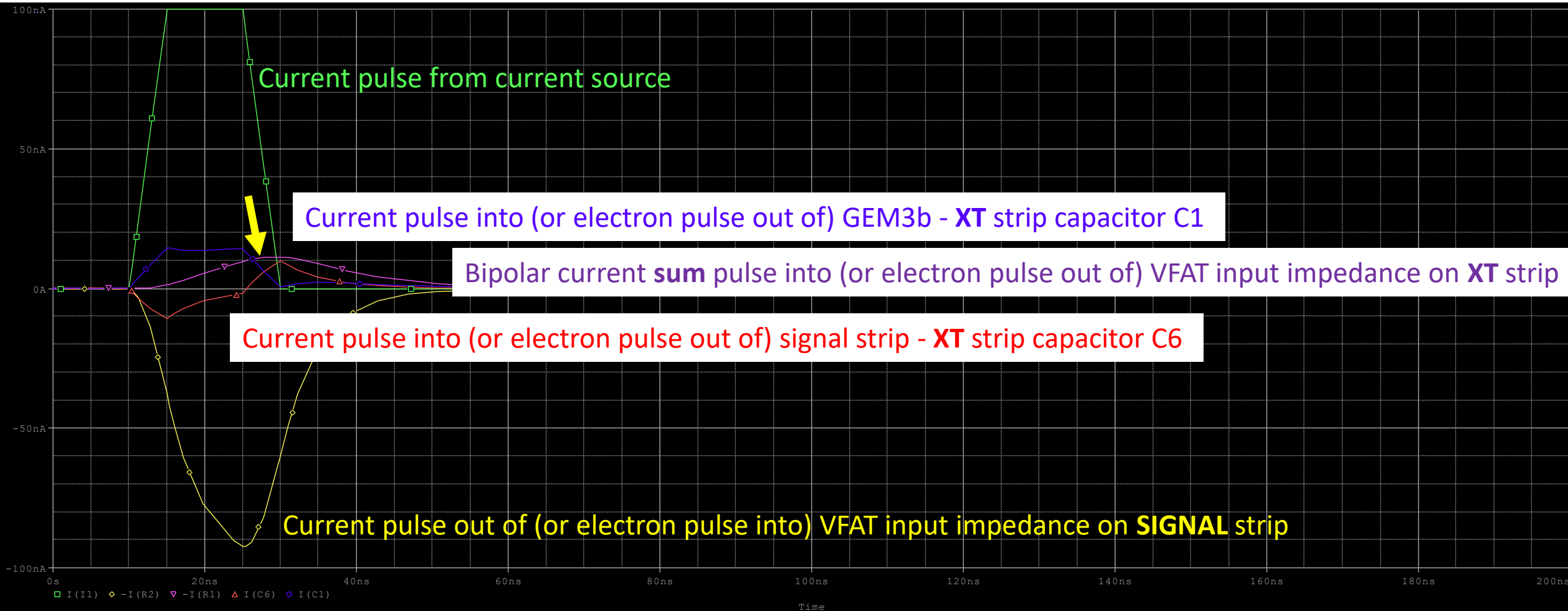


# Mitigation strategies: Overcoming Limitations?

- Let's probe and compare the two contributions to the XT current through the interstrip capacitance C6 and the GEM3b-strip capacitance C1:



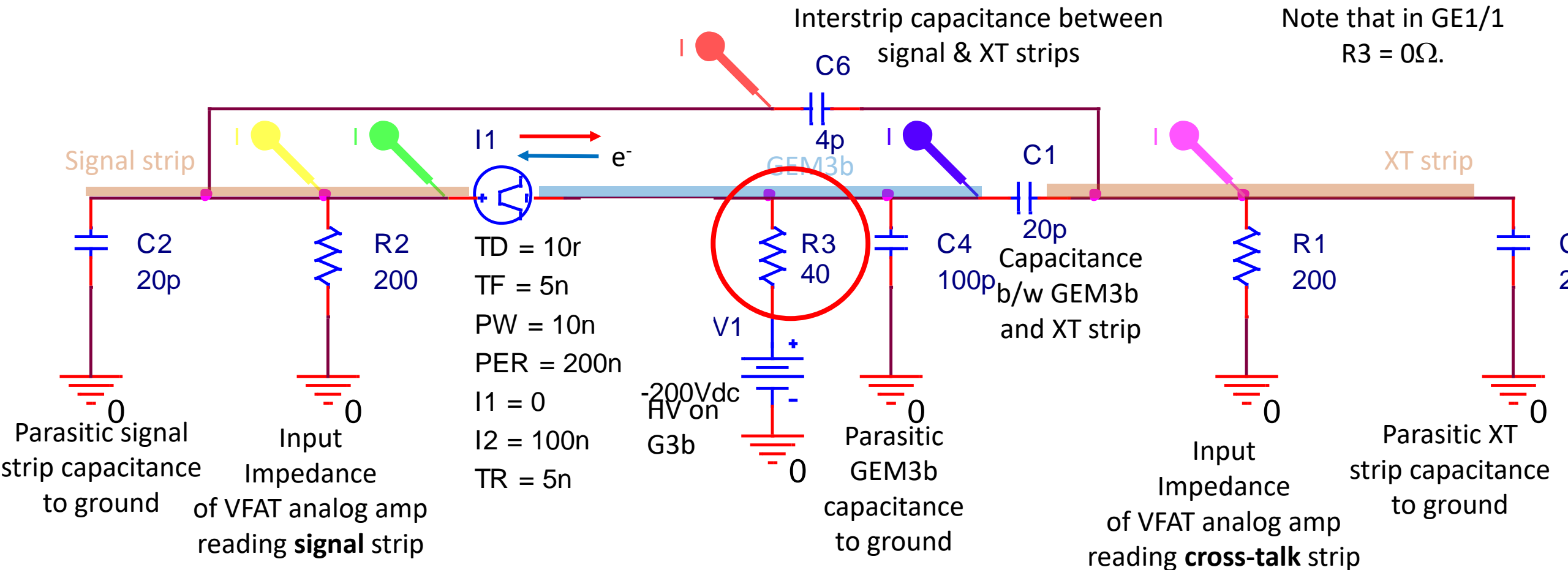
# Mitigation strategies: Overcoming Limitations?



**Main observation:** The two XT contributions have **opposite polarity** as they are connected to opposite ends of the current source ! *If only they cancelled out...*

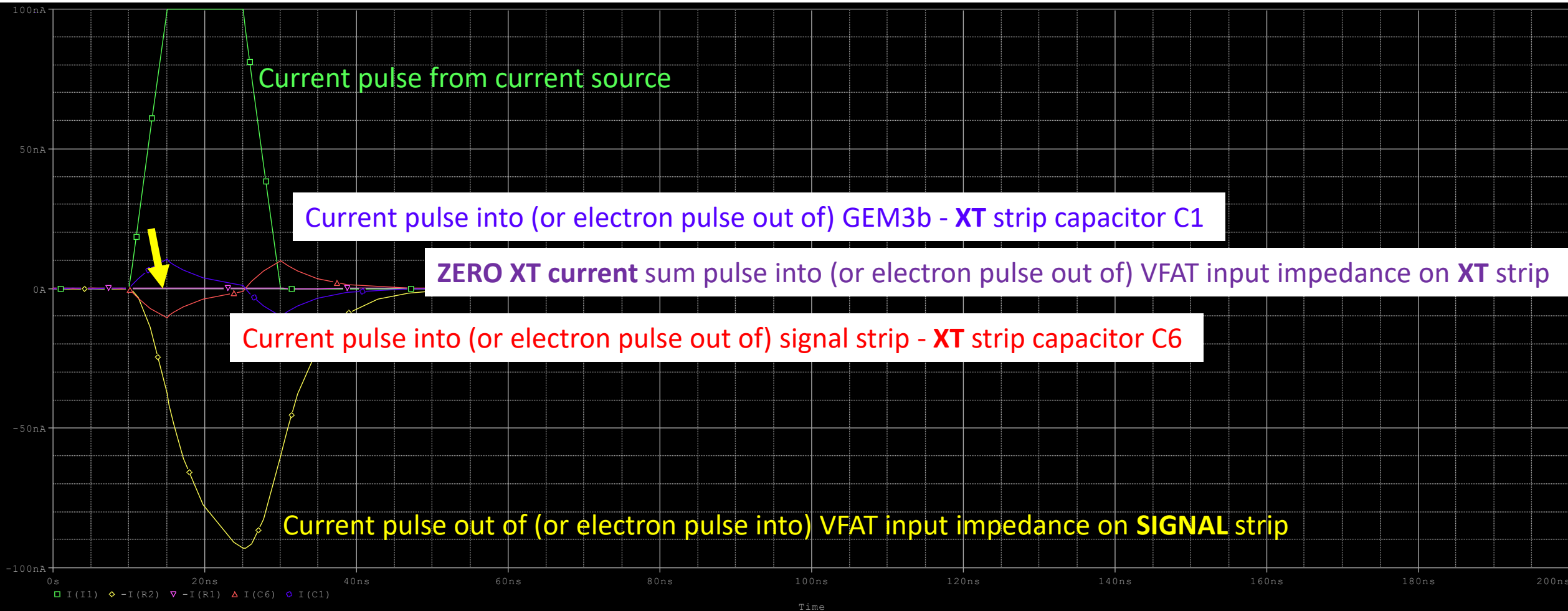
# Mitigation strategies: Overcoming Limitations?

- Well, for a particular value of the protection resistor R3 (40Ω) you CAN actually sink away just enough current so that the two crosstalk currents DO CANCEL:





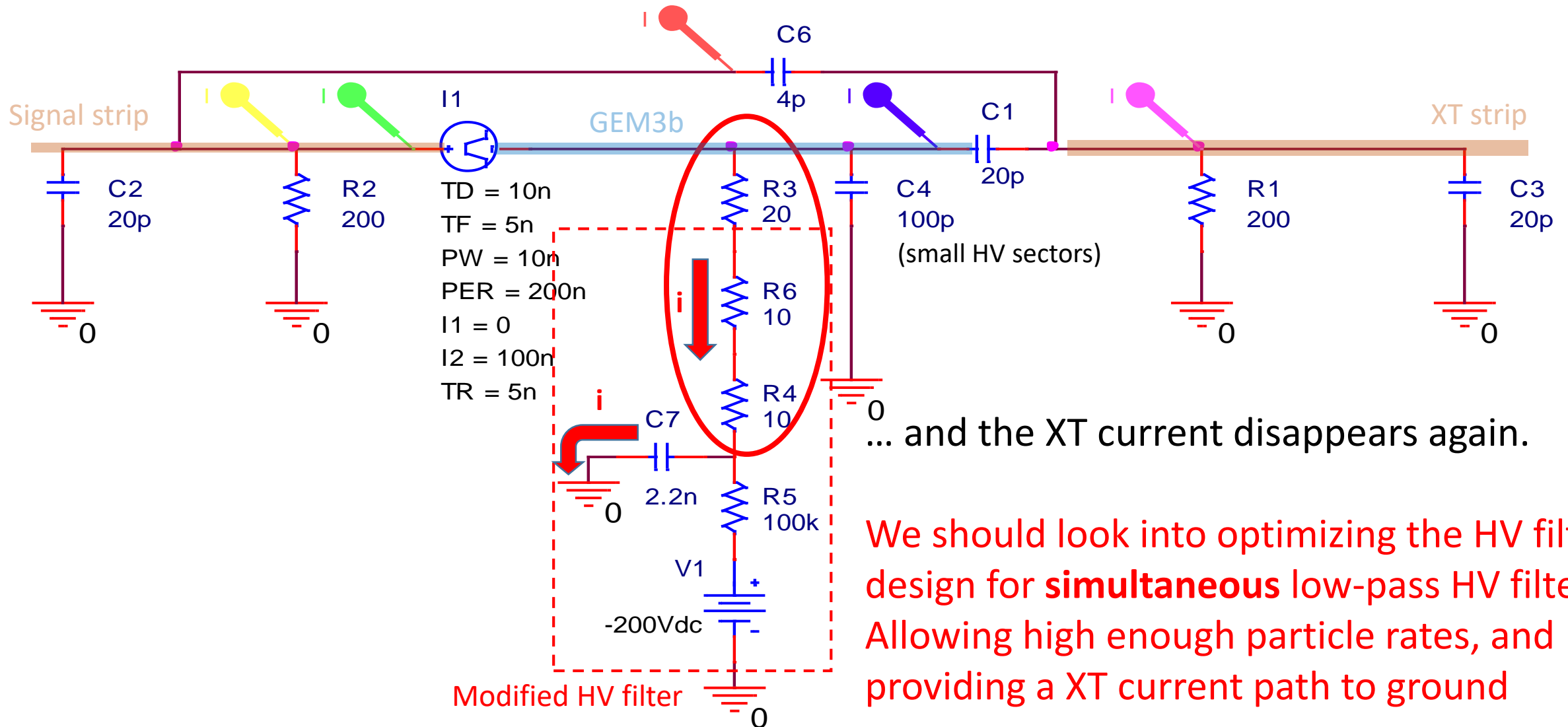
# Mitigation strategies: Overcoming Limitations?



**Main observation:** The two XT contributions have opposite polarity and **cancel out**.  
The netXT current is **zero!** The signal current is unaffected.

# Mitigation strategies: Implement in HV filter?

- With a small R3 protection resistor and modified HV filter, again  $R_{tot} = 40 \Omega$ :



# XT mitigation vs. Discharge protection

It appears that crosstalk mitigation and protection against discharge damage of the readout unfortunately oppose each other:

- Increasing the capacitance of GEM3b reduces XT, but increases the charge and energy of discharges into the VFATs
- Introducing bypass capacitors reduces XT, but provides an additional source of charge that can discharge into the readout
- Reducing protection resistance reduces XT, but also reduces discharge protection.

Mitigation of both effects has to be carefully balanced in the final GEM foil design and experimentally validated. See also Jeremie's and Davide's talks.

# Long Summary & Conclusions

## Results from the PSPICE model of the GEM crosstalk circuit

- replicate experimental XT results obtained with a voltage pulser at FIT
- explain why tests with a voltage pulser produce *same-sign* XT pulses while tests with a GEM in normal operation produce *opposite-sign* XT pulses as due to the difference between an external voltage source and an internal current source
- show that any method for reducing the *impedance  $Z$  of GEM3-b to ground* will reduce XT:
  - GEM3b foil segments with larger capacitance ( $Z = 1/\omega C$ )
  - connection of GEM3b foil without protection resistor (as in GE1/1)
  - bypass capacitor on 100k $\Omega$  protection resistor
- show that this mitigation has no significant impact on signal integrity
- show that additional devices upstream of a large protection resistor will be ineffective
- caution that the mitigation of this “GEM3-bottom to ground impedance” has its limits due to the additionally present impedance from the interstrip capacitance
- show that XT can be expected to be reduced by up to a factor  $\approx 4$  by this type of mitigation
- show that by reducing the protection and HV filter resistances, the GEM3-bottom to ground impedance XT and the interstrip capacitance XT can cancel each other and net XT becomes zero
- demonstrate a need for careful balancing of discharge mitigation and XT mitigation

# Short Summary & Conclusions

## Results from the PSPICE model of the GEM crosstalk circuit

- provide qualitative and quantitative understanding of our experimental XT results
- establish that the observed XT is due to capacitive coupling
- inform our mitigation strategies
- show that there is tension between XT mitigation and discharge protection

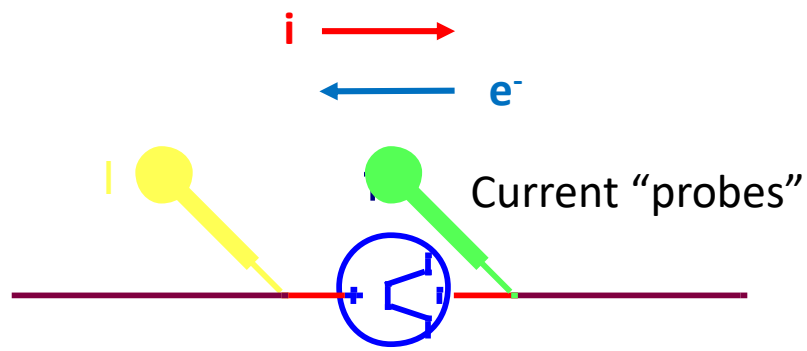
# Thank you!

The End

# Backup

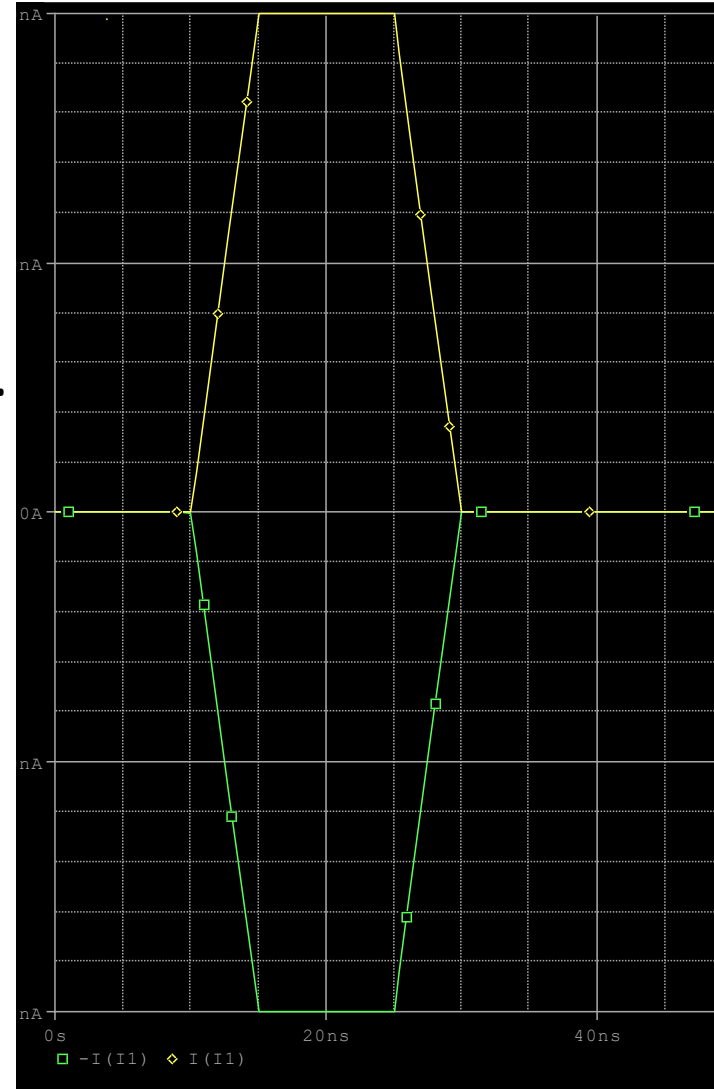
# PSPICE Current convention: Example

## Pulsed current source:



$TD = 10n$   
 $TF = 5n$   
 $PW = 10n$   
 $PER = 200n$   
 $I1 = 0$   
 $I2 = 100n$   
 $TR = 5n$

Current flows **into** source on the left and is counted **pos.**



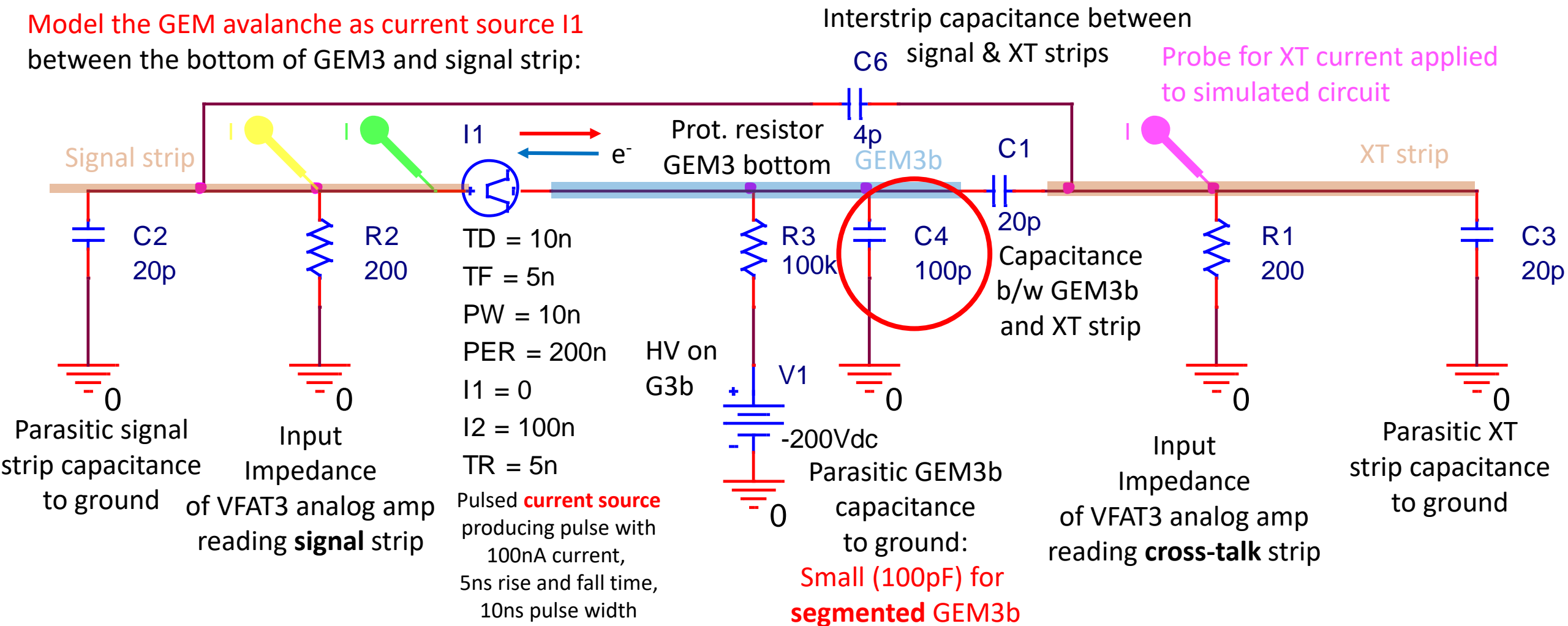
Current flows **out of** source on the right and is counted **neg.**

*But it is of course one and the same current !*



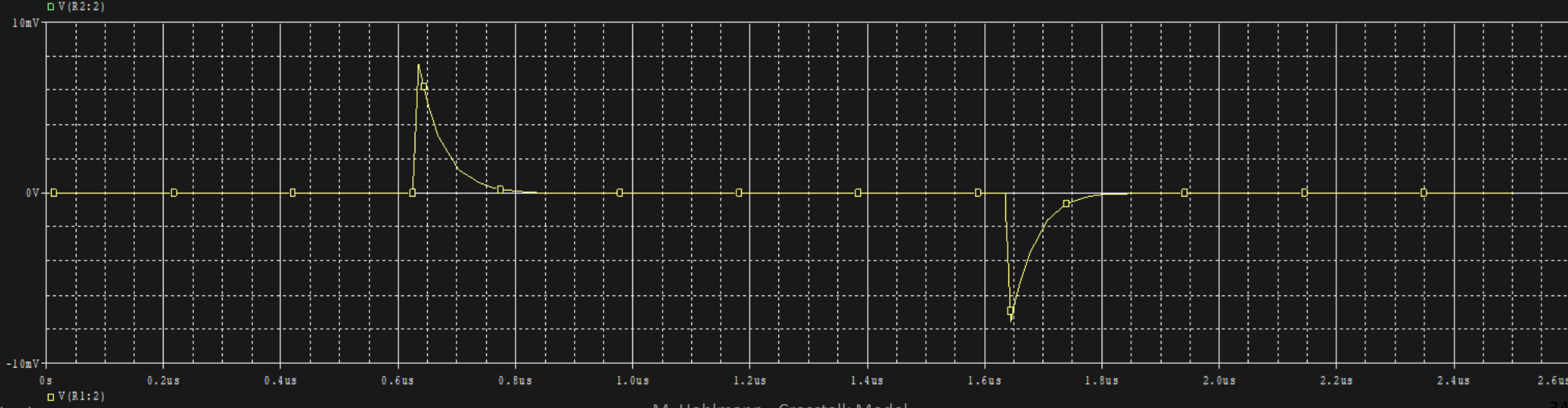
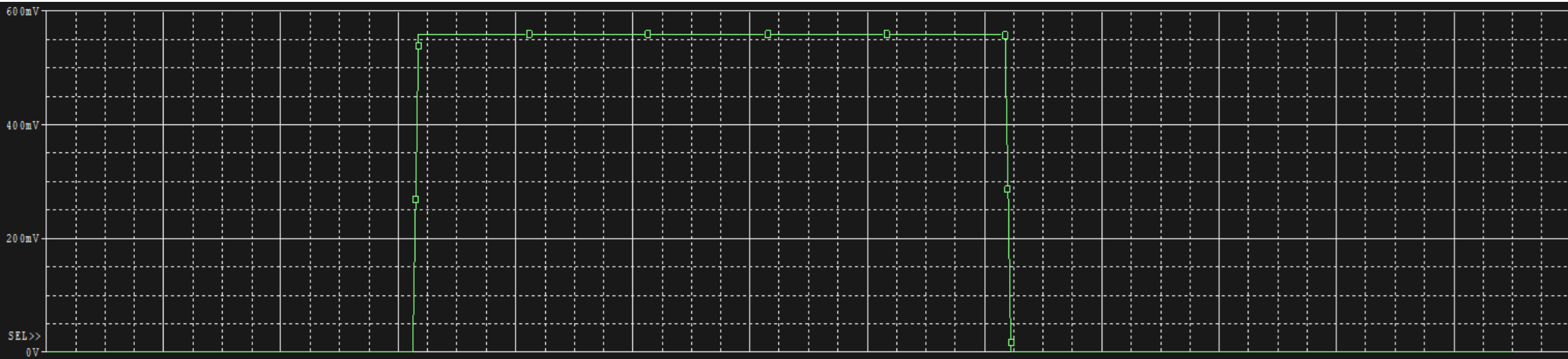
# 2. PSPICE circuit implementation for gas avalanche

Model the GEM avalanche as current source I1 between the bottom of GEM3 and signal strip:



Current source: 10,000 primary electrons (1.6 fC) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$  (note that this doesn't even take gas gain into account)

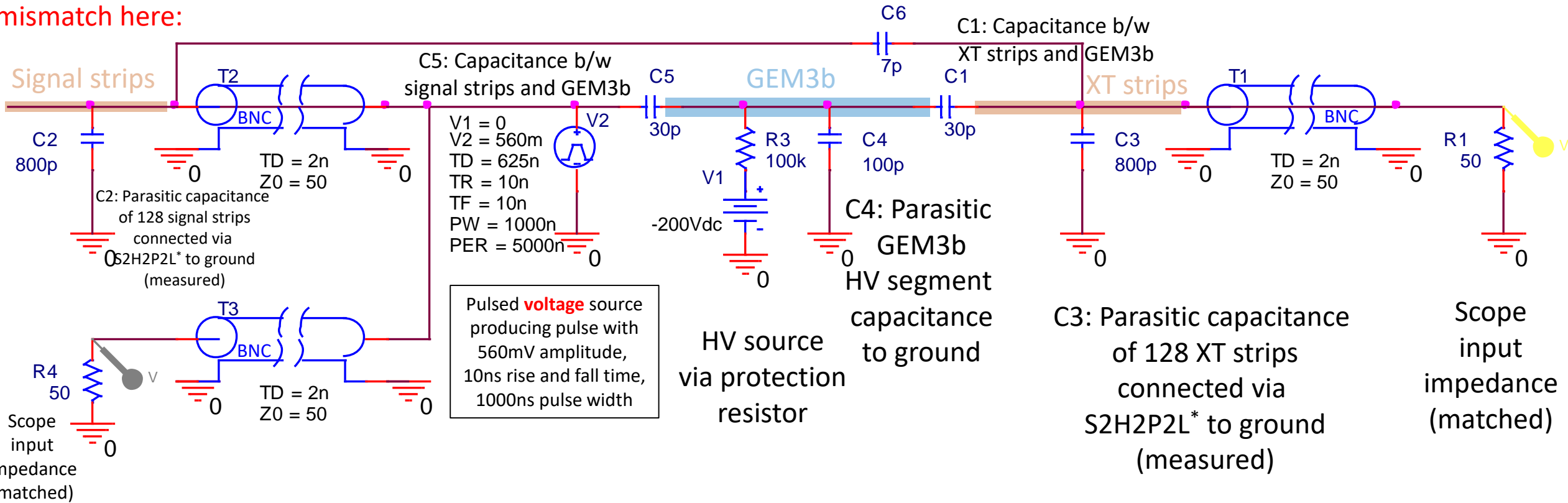
# Zoom of simulation output on p.5



# 1. More detailed circuit for pulser measurements

Include the transmission lines (50 Ohm BNC cables) used in the actual measurements:

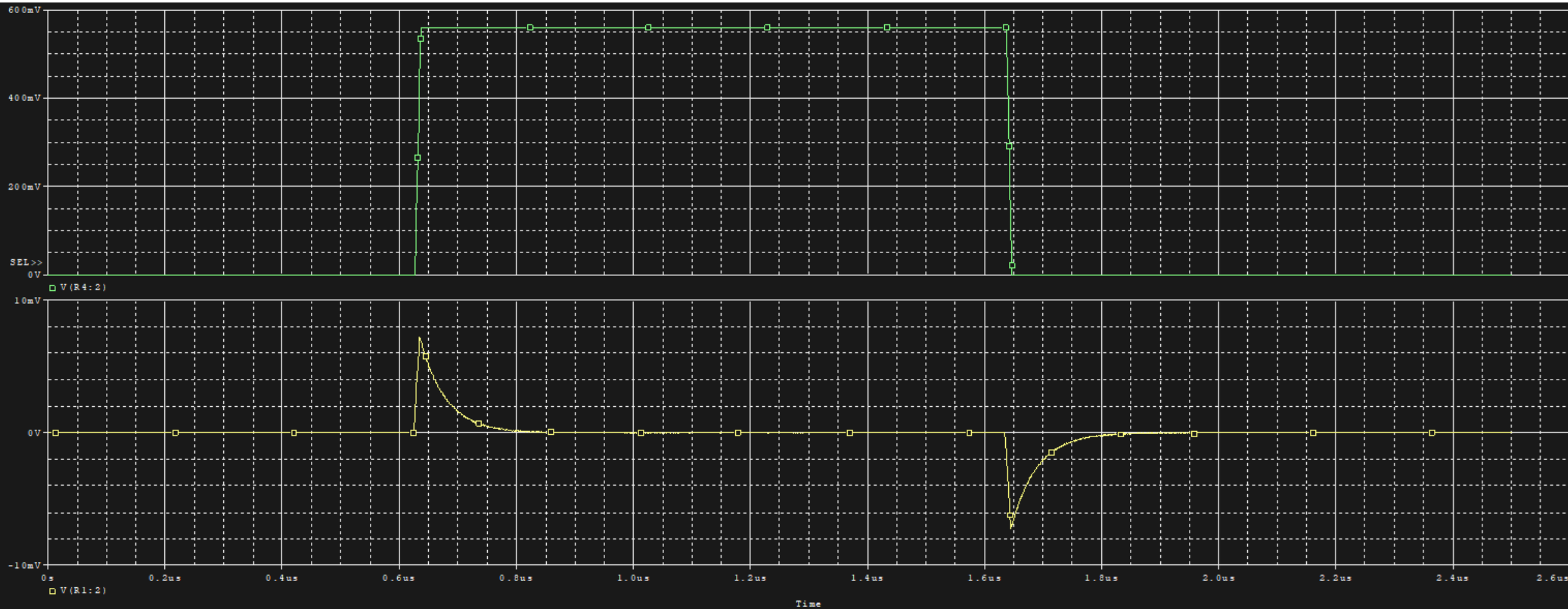
Worried about impedance mismatch here:



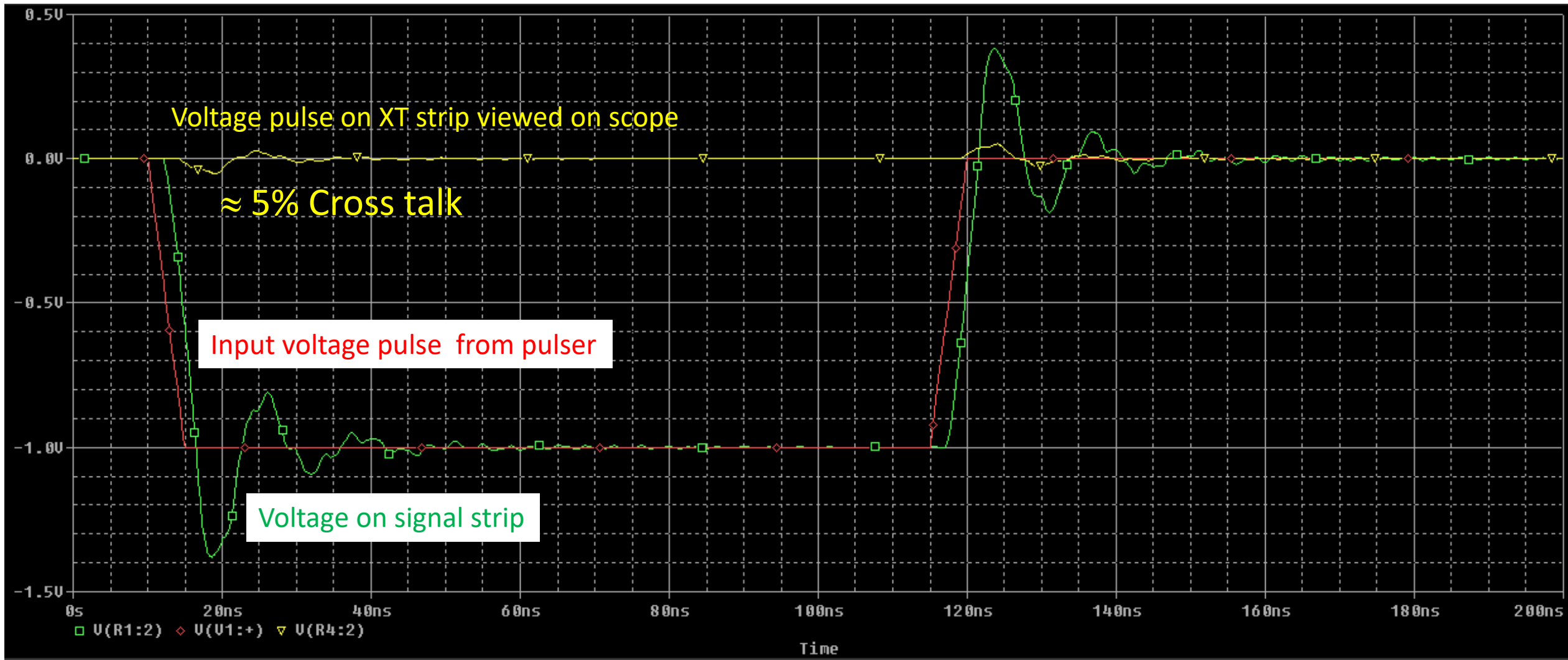
**RESULTS:** Turns out results are identical to the simulation with the simplified circuit on pp. 4/5

\* "Strip to Hirose to Panasonic to LEMO" adapter

# 1. More detailed circuit for pulser measurements



# 1. Pulse analysis for pulser measurements



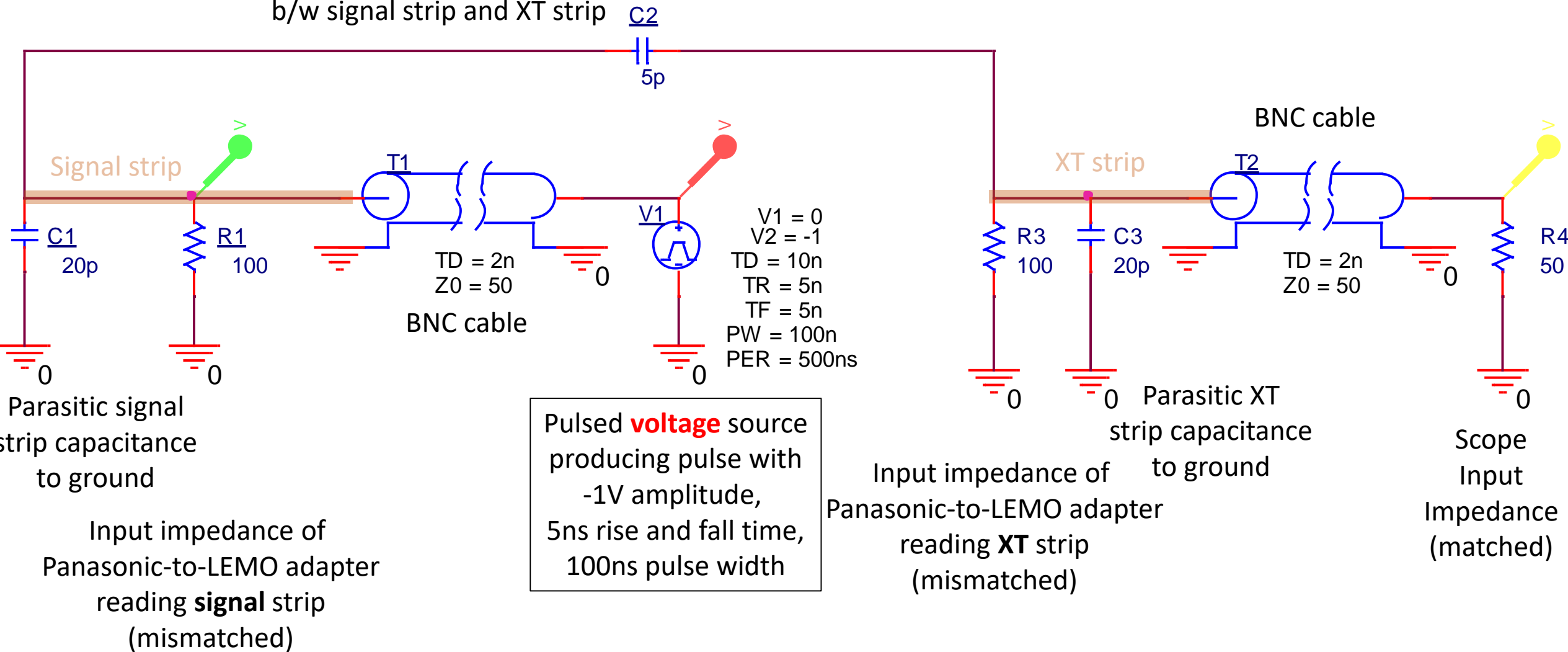
## Main observation:

- Cross talk voltage pulse, input voltage pulse, and voltage pulse on signal strip all **have THE SAME POLARITY on leading edge**
- Cross talk pulse is bipolar

# Older Model Circuit for pulser measurements

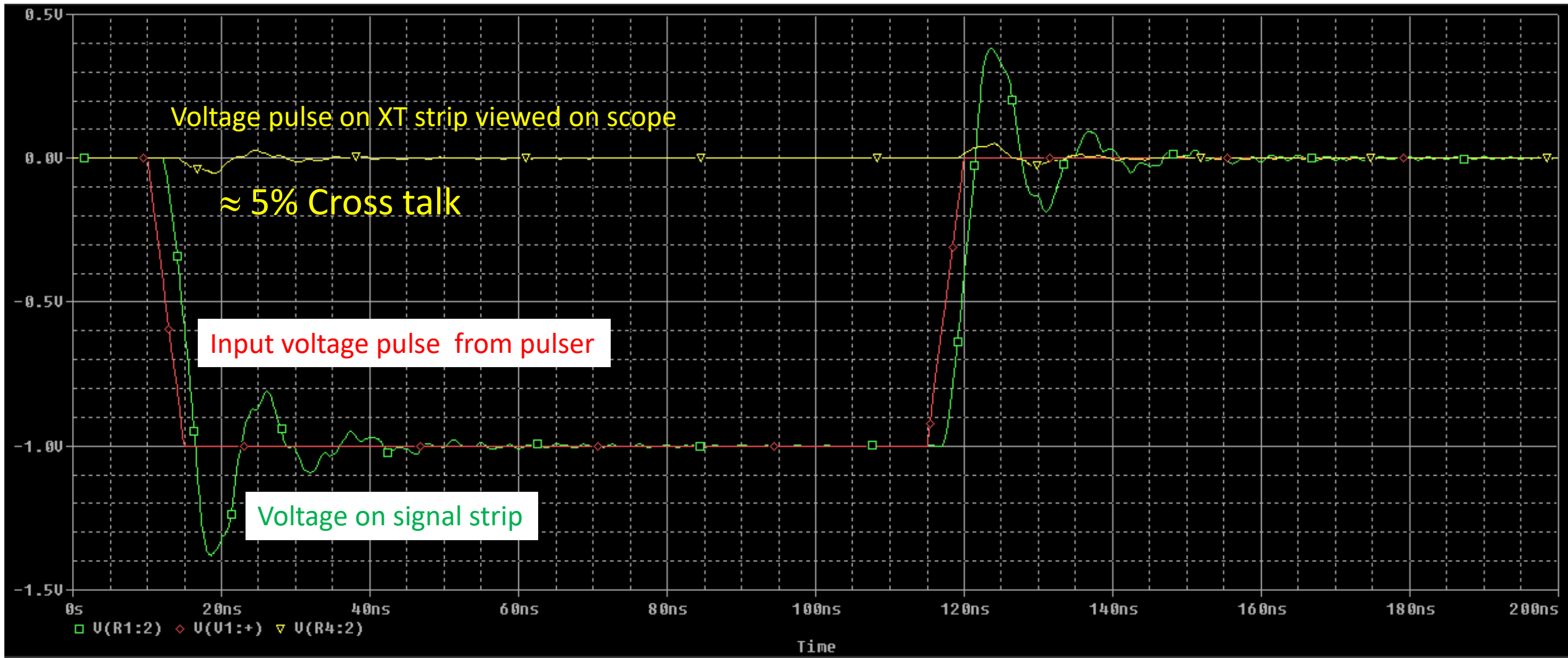
For Stephen's measurements with voltage pulser at FIT

Interstrip Capacitance  
b/w signal strip and XT strip



Pulsed **voltage** source  
producing pulse with  
-1V amplitude,  
5ns rise and fall time,  
100ns pulse width

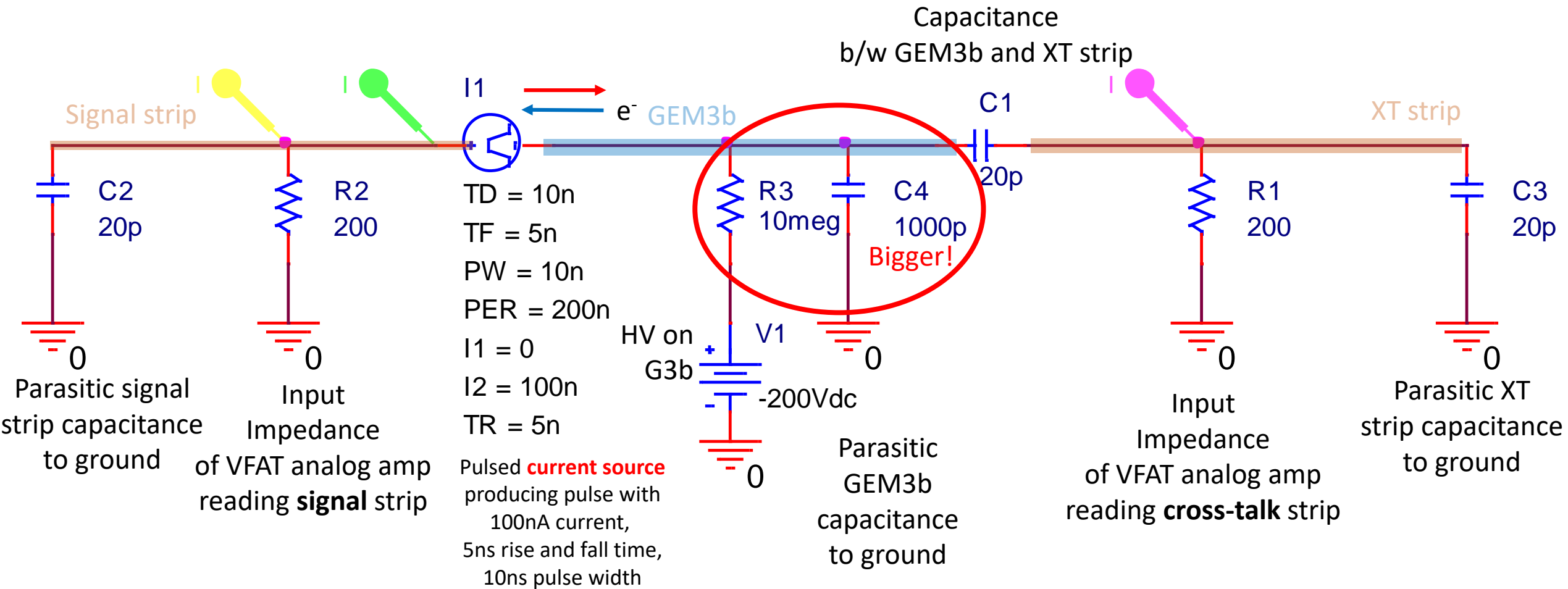
# 0. Pulse analysis for pulser measurements



## Main observation:

- Cross talk voltage pulse, input voltage pulse, and voltage pulse on signal strip all **have THE SAME POLARITY** on leading edge
- Cross talk pulse is bipolar

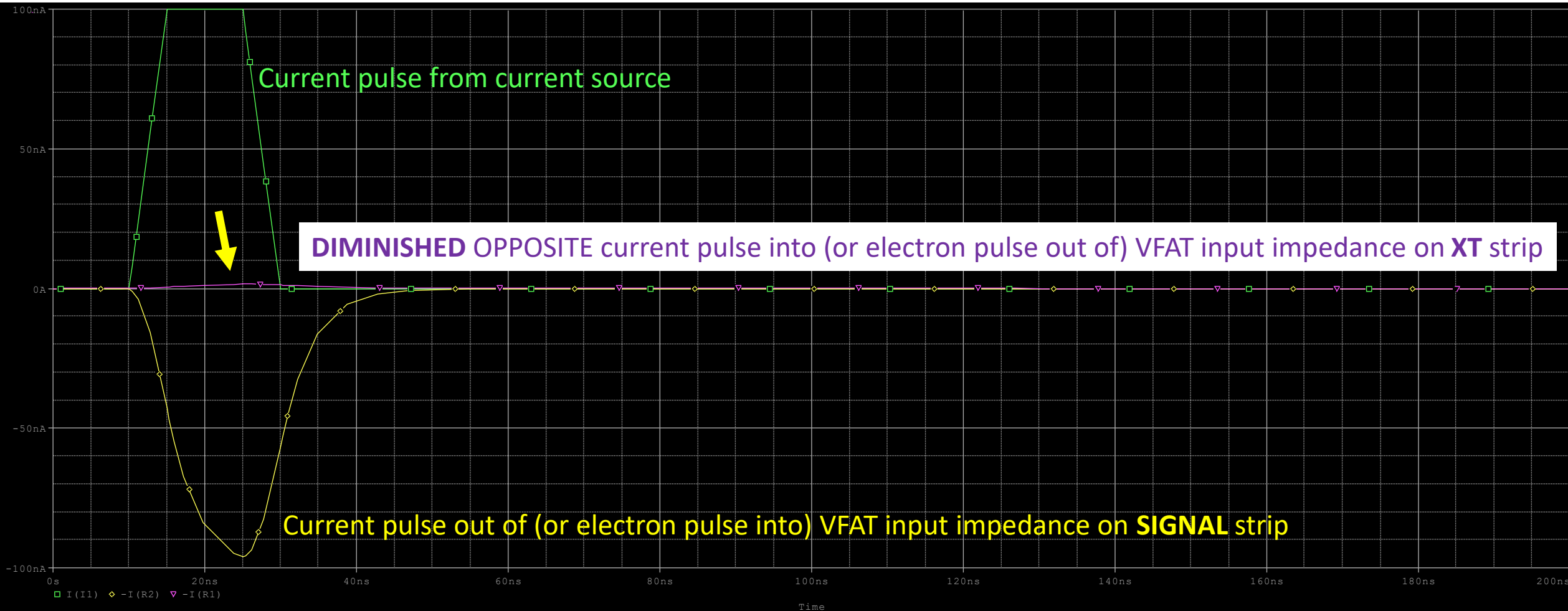
# n. Single-segmented foil: Large cap., large $R_{prot}$



Current source: 10,000 primary electrons (1.6 fC) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$   
 (note that this doesn't even take gas gain into account)

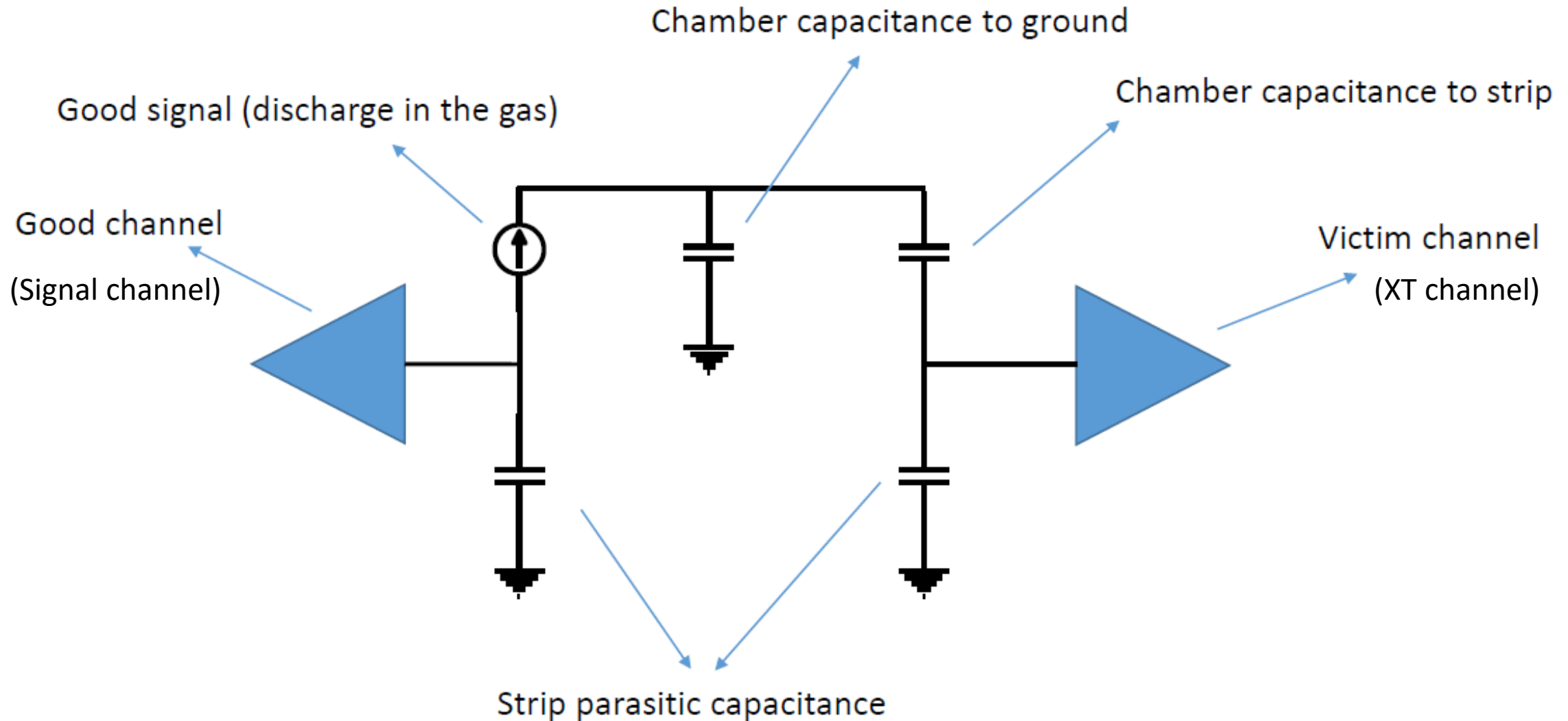


# n. GE1/1 foil: Single-segmented, large cap.



**Main observation: OPPOSITE polarity XT pulse is DIMINISHED!**

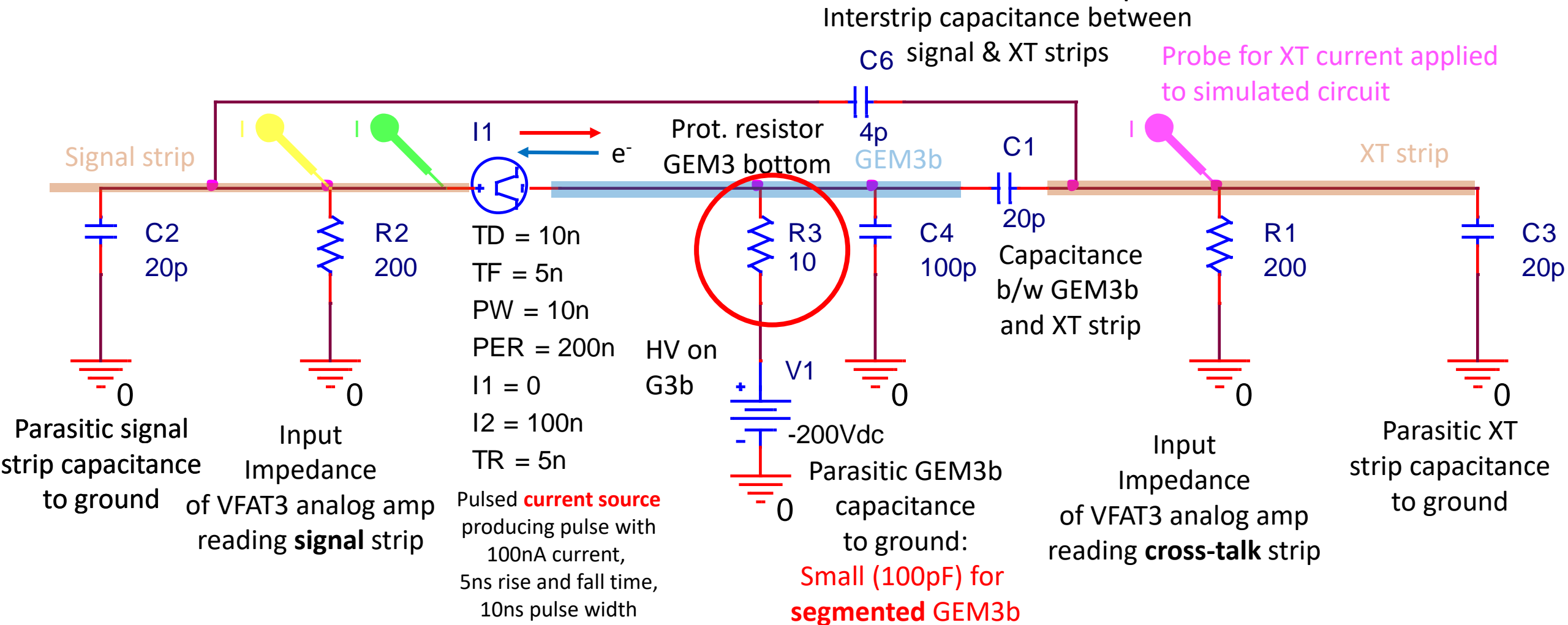
# Guided by Francesco Licciulli's model:



# The PSPICE Current Sign Convention

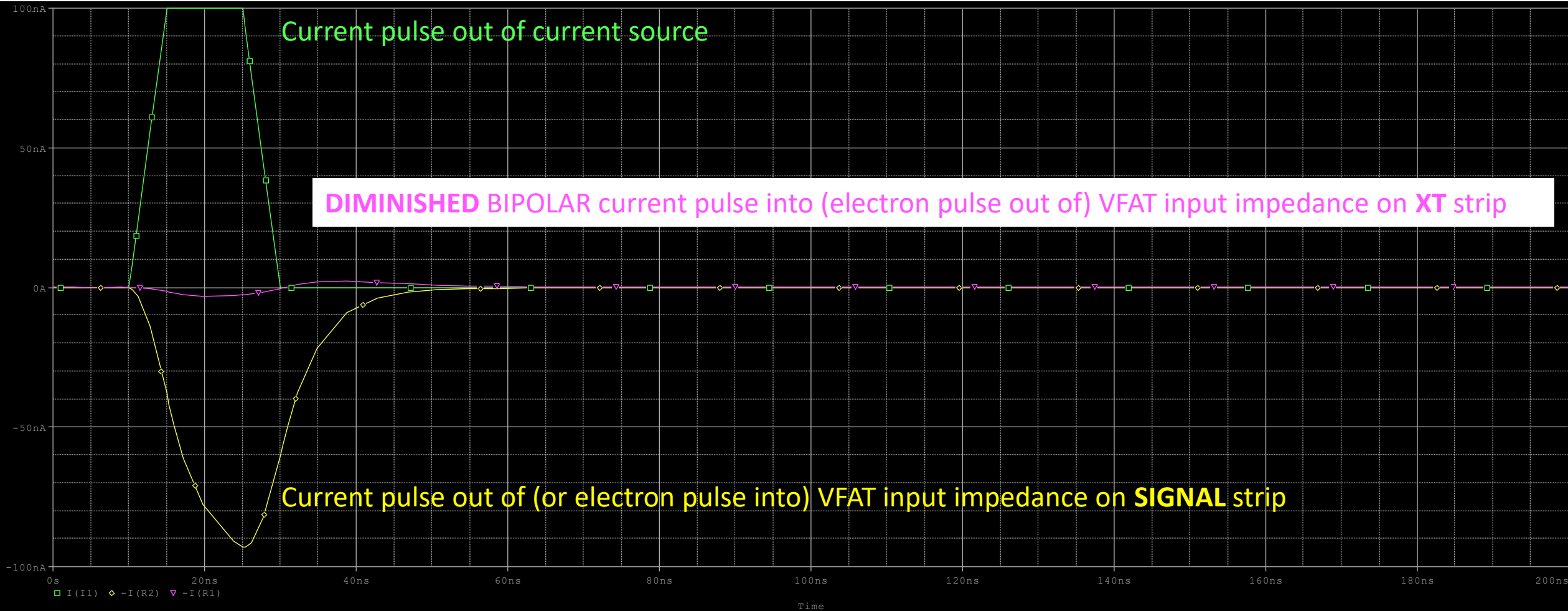
- Voltage polarities are easy to understand because they simply have one value relative to GRD
- Currents are bit more tricky since they also have a direction
- The direction or sign of a current in PSPICE is measured **relative to a device**
- The **PSPICE convention for current polarity** is this:
  - The current is probed at one terminal (“pin”) of a device (R,C,...)
  - **If at that terminal the current flows INTO the device, it is counted POSITIVE**
  - If at that terminal the current flows OUT OF the device, it is counted NEGATIVE
  - “Current” here refers to technical current, i.e. flow of positive charges; electron flow would be in the opposite direction

# 3. Circuit for avalanche with $R3 = R_{prot} = 10 \Omega$



Current source: 10,000 primary electrons (1.6fc) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$   
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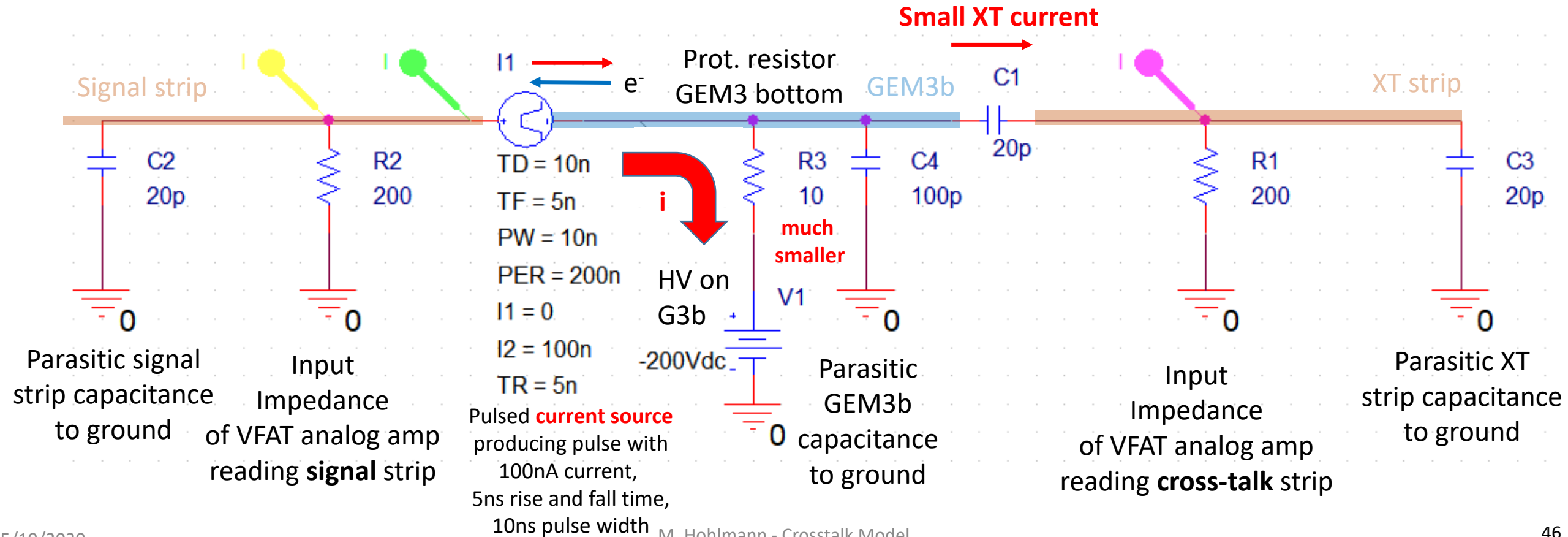
# 3. Pulse Analysis for avalanche with $R3 = R_{prot} = 10 \Omega$



**Main observation: The XT pulse is DIMINISHED by a factor  $\approx 4$  and becomes bipolar!**

# Making sense of the results

- In this circuit, the artificially reduced resistance of the protection resistor provides a **much reduced impedance for sinking the current from the current source to ground.**
- As a consequence, the amount of XT current that can flow into C1 is reduced.
- **This explains why XT is observed on double-segmented foils, but not on single-segmented foils!**



# Mitigation strategies: Increase GEM3b cap.

- Now that we have a better understanding of how the XT is produced, we can investigate mitigation strategies with the simulation
- **Sinking more current from GEM3b to ground is important to reduce XT.** However, we presumably don't want to reduce our HV protection resistance on GEM3b too much for safety reasons.
- Instead, we would expect to be able to sink more current also by **reducing the impedance Z of the parasitic capacitance C4 between GEM3b and ground**
- Since  $Z = 1/(\omega C)$ , we need to **increase** that parasitic capacitance to reduce Z
- Lets increase C4 from 100pF to 1000pF...

# Possible implementation (Jeremie's talk one week ago):

## Anticipating a possible solution

- Most promising option so far is to increase HV size (we don't introduce new elements and we don't change the basic settings of detector or electronics)
- Problematic: it can bring back discharge propagation issue

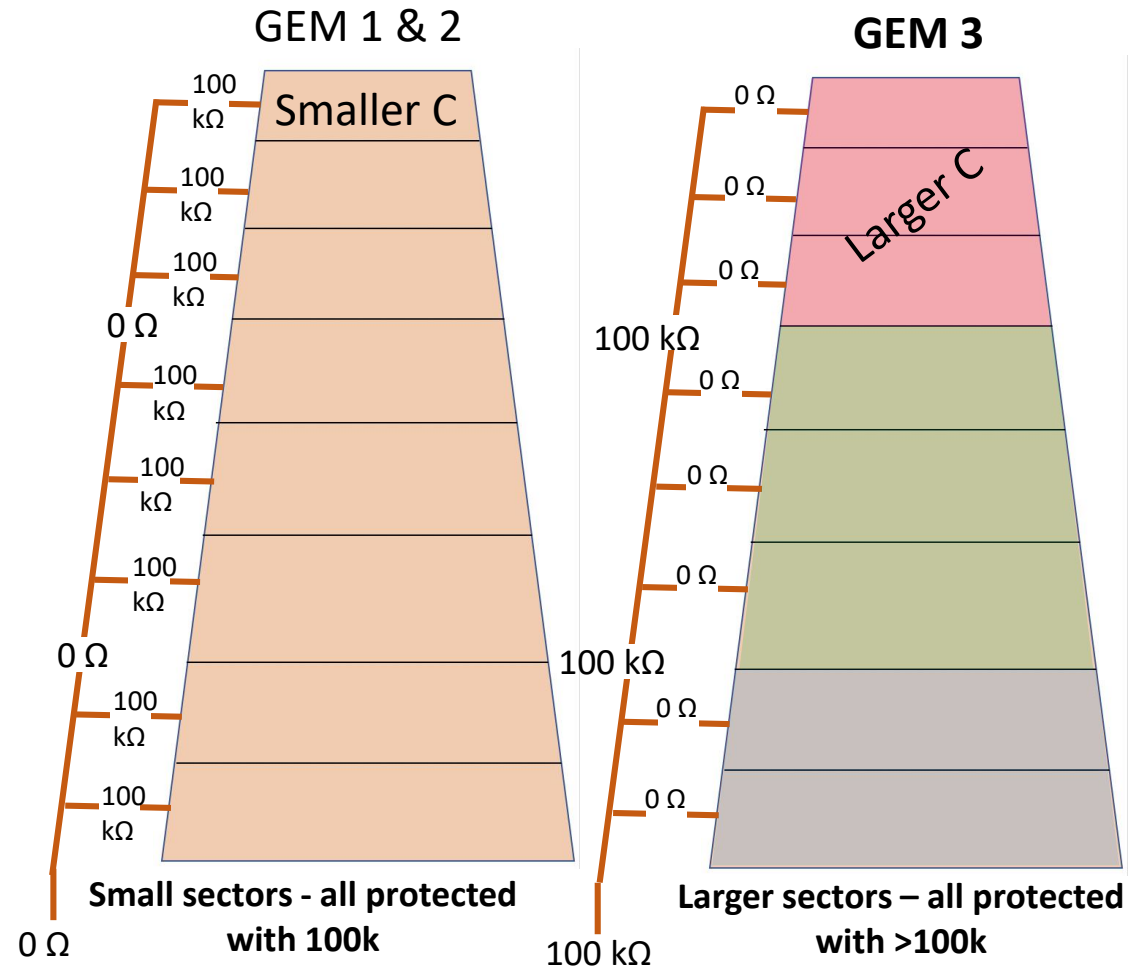
*How to mitigate that:*

Use a unique layout but with multiple resistor options

- use fine segmentation on GEM1 and GEM2 to stop propagation
- use coarse segmentation on GEM3 to prevent crosstalk

→ Decoupling capacitor on the electronics side might be mandatory to fully stop the propagations

Same layout (i.e. production mask) for all three foils  
Minor modifications with respect to current design



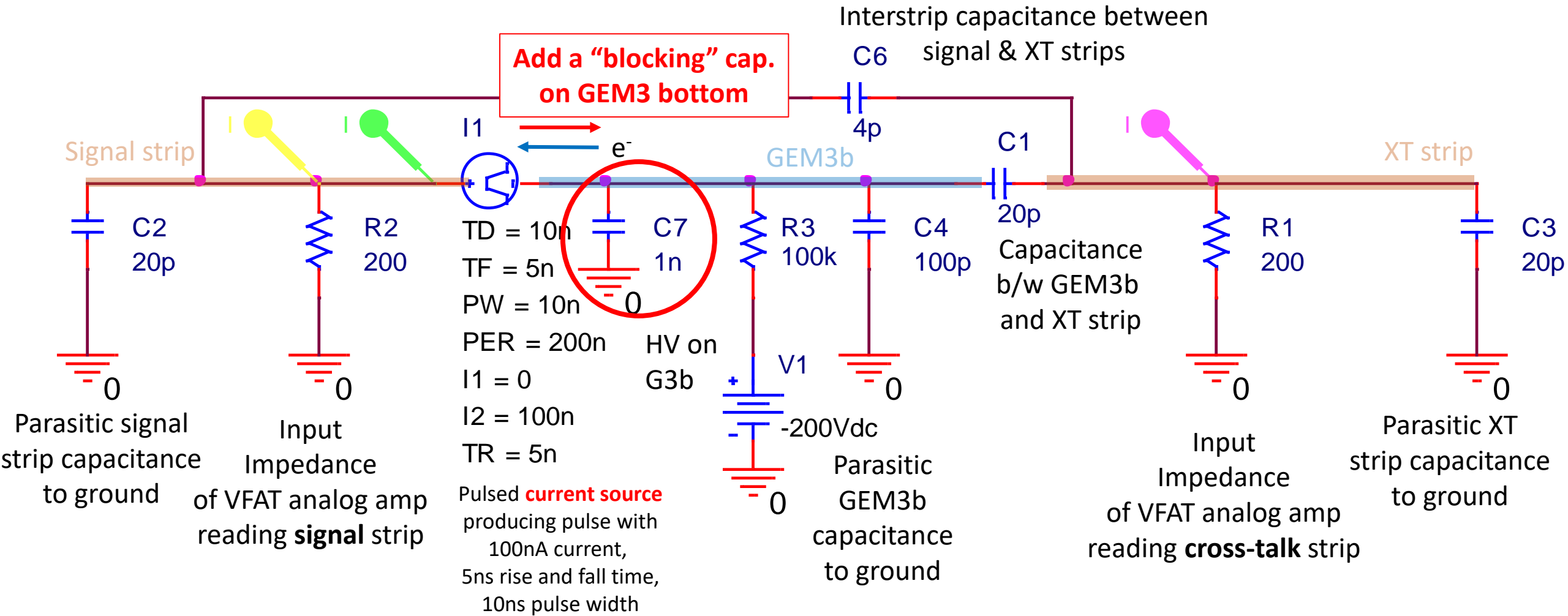
JM



# Mitigation strategies: “Blocking” Capacitor

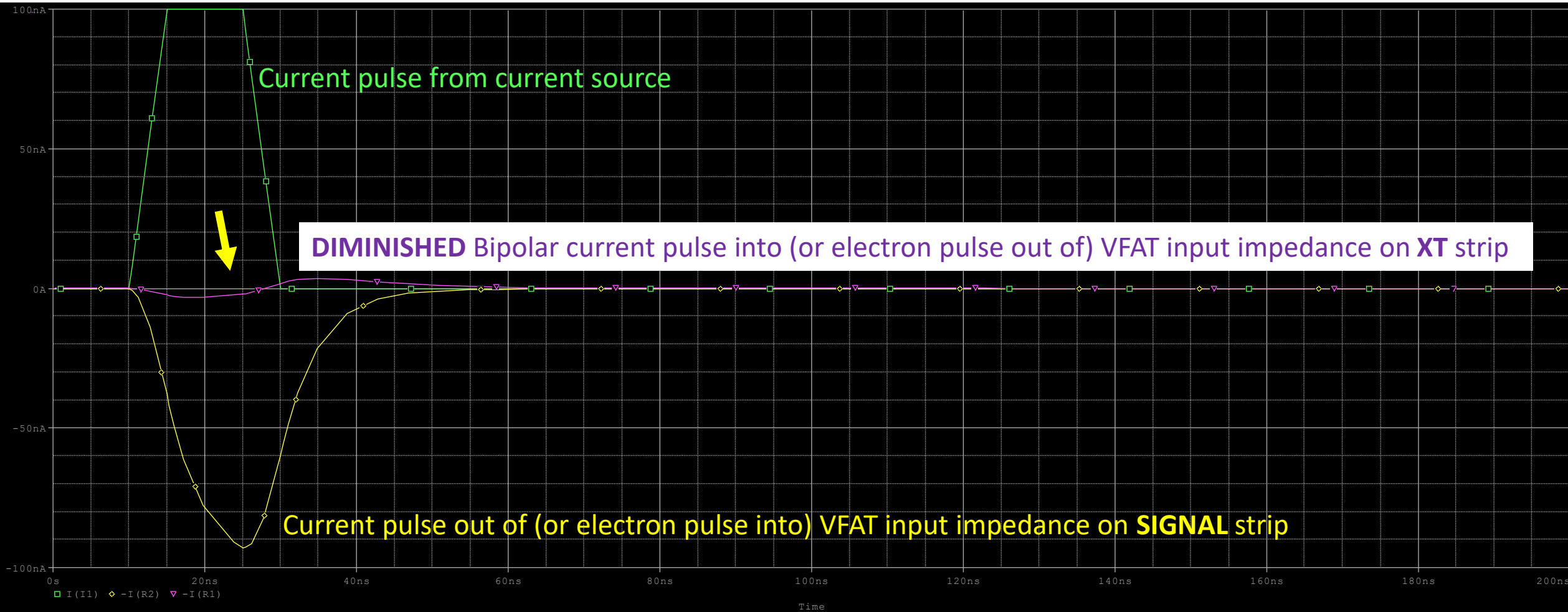
- Another strategy that has been suggested is to put a “**blocking**” **capacitor on GEM3b** that will provide an additional path to ground for the AC current pulse from GEM3b (but not for DC, i.e. HV)
- This will also decrease GEM3b impedance to ground
- Let’s place such a capacitor with  $C_5 = 1000\text{pF} = 1\text{nF}$

# 6. Place a “blocking” cap. on GEM3b



Current source: 10,000 primary electrons (1.6 fC) over 15 ns:  $i = 10^4 \cdot 1.6 \cdot 10^{-19} \text{ C} / 15 \cdot 10^{-9} \text{ s} = 10^{4-1-19+9} = 10^{-7} \text{ A} = 100\text{nA}$   
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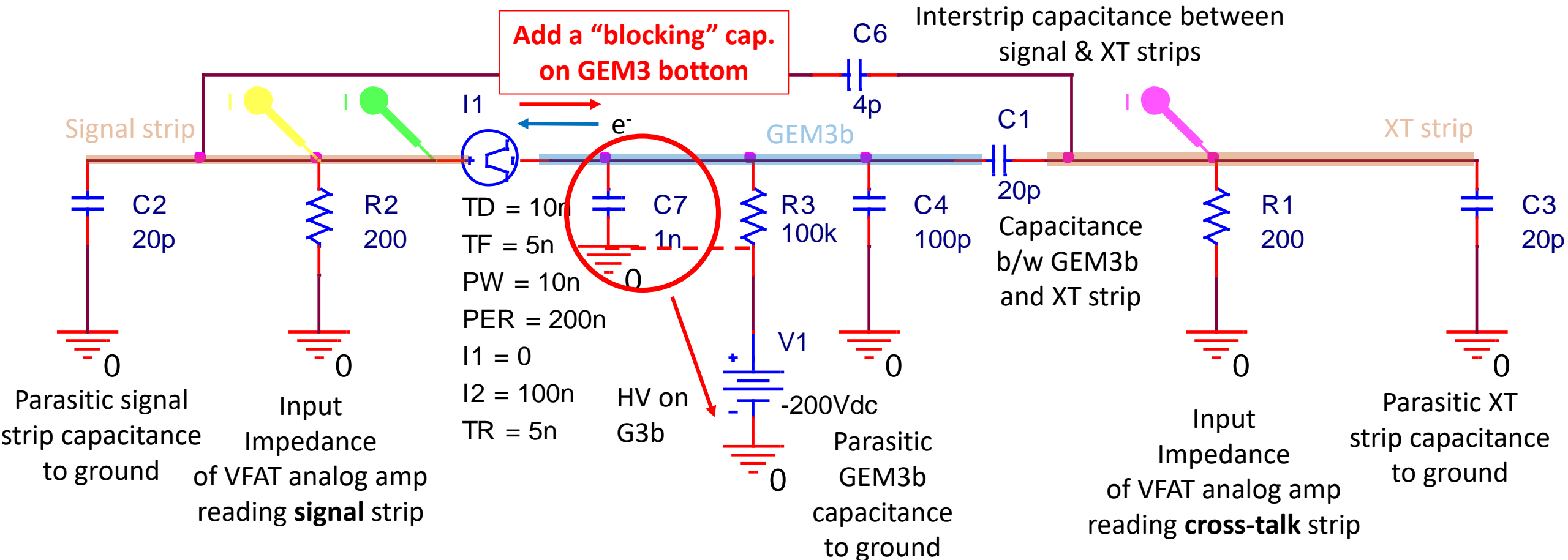
# 6. Place a “blocking” cap. on GEM3b



**Main observation: OPPOSITE polarity XT pulse is AGAIN DIMINISHED!**

# Mitigation strategies: “Blocking” Capacitor

- This is actually not that surprising because for AC current the HV voltage source V1 acts like a ground, so this is **essentially equivalent** to placing a bypass capacitor in parallel on R3:

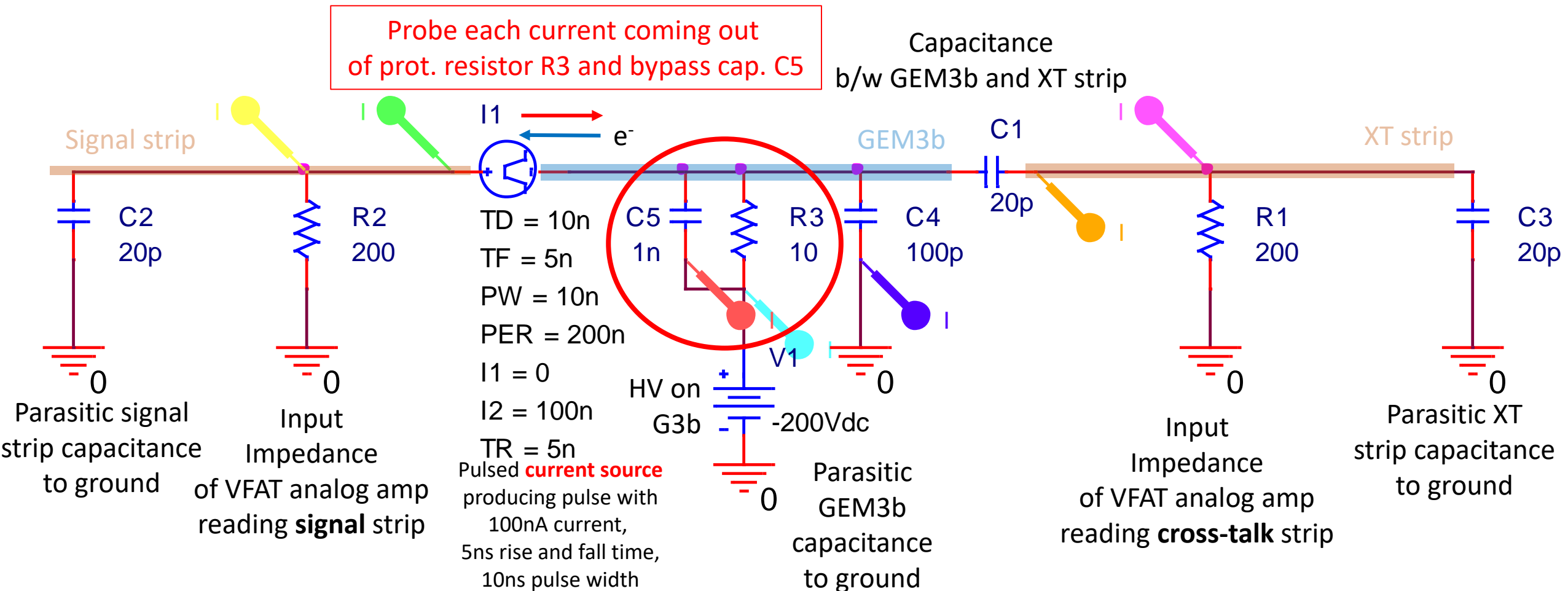


# Academic's curiosity:

- Just because we are curious, let's see for what value of the protection resistor we get **the same amount of sinking current through the protection resistor and the bypass capacitor** around it.
- Let's change  $R_{\text{prot}} = R_3$  back to  $10 \Omega$  because then resistor and  $1\text{nF}$  bypass capacitor  $C_5$  have equal impedances at  $100 \text{ MHz}$  ( $10 \text{ nF}$  pulse width):

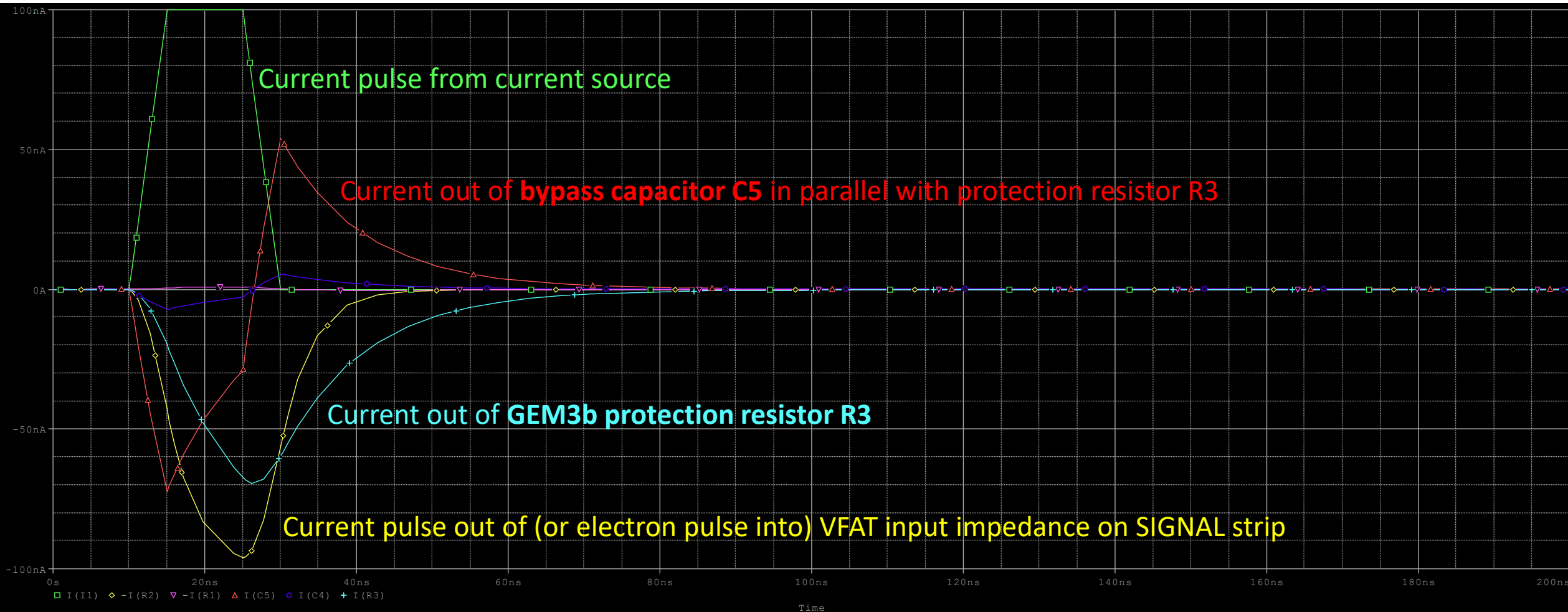
$$10 \Omega = R_3 \approx 1/\omega C_5 = 1/(100 \text{ MHz} \cdot 1 \text{ nF}) = 1/(10^8 \cdot 10^{-9}) = 10 \Omega$$

# 6. Let impedance of bypass cap $\approx R_{\text{prot}}$ on GEM3b



Equal impedances:  $10 \Omega = R_3 \approx 1/\omega C_5 = 1/(100 \text{ MHz} \cdot 1 \text{ nF}) = 1/(10^8 \cdot 10^{-9}) = 10 \Omega$

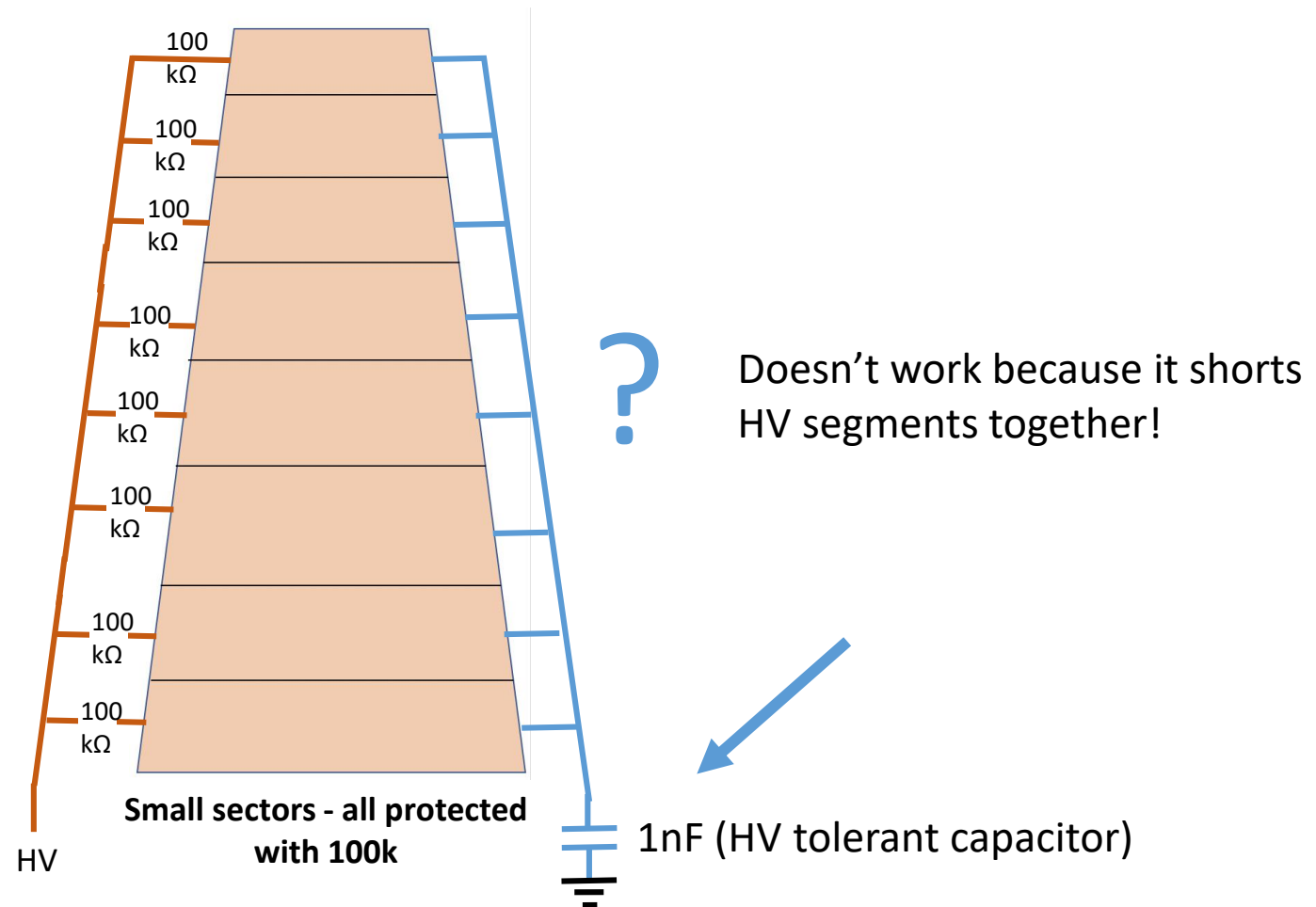
# 6. Impedance of bypass cap $\approx R_{\text{prot}}$ on GEM3b



**Main observation:** The amplitudes of the currents out of the protection resistor R3 and the bypass capacitor C5 are indeed equal because they have equal impedances around  $\omega = 100$  MHz (corresponding to 10ns pulse width)

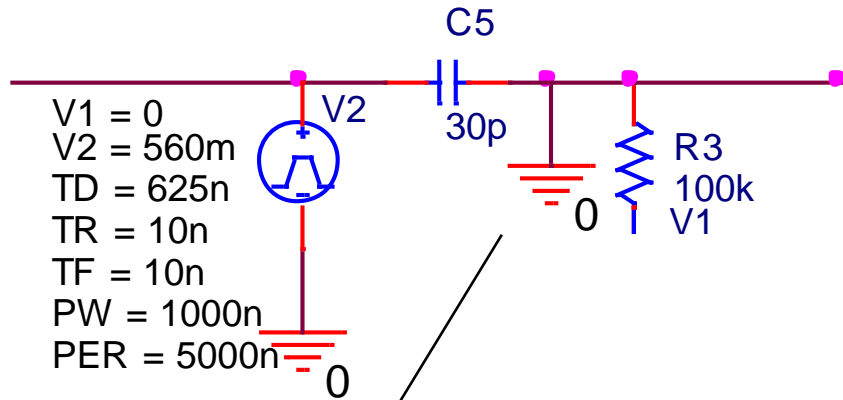
# Mitigation strategies: “Blocking” Capacitor?

- Maybe this can be done with a **single** device **on the “other side”** of the HV segments (unless there are already traces and components there):





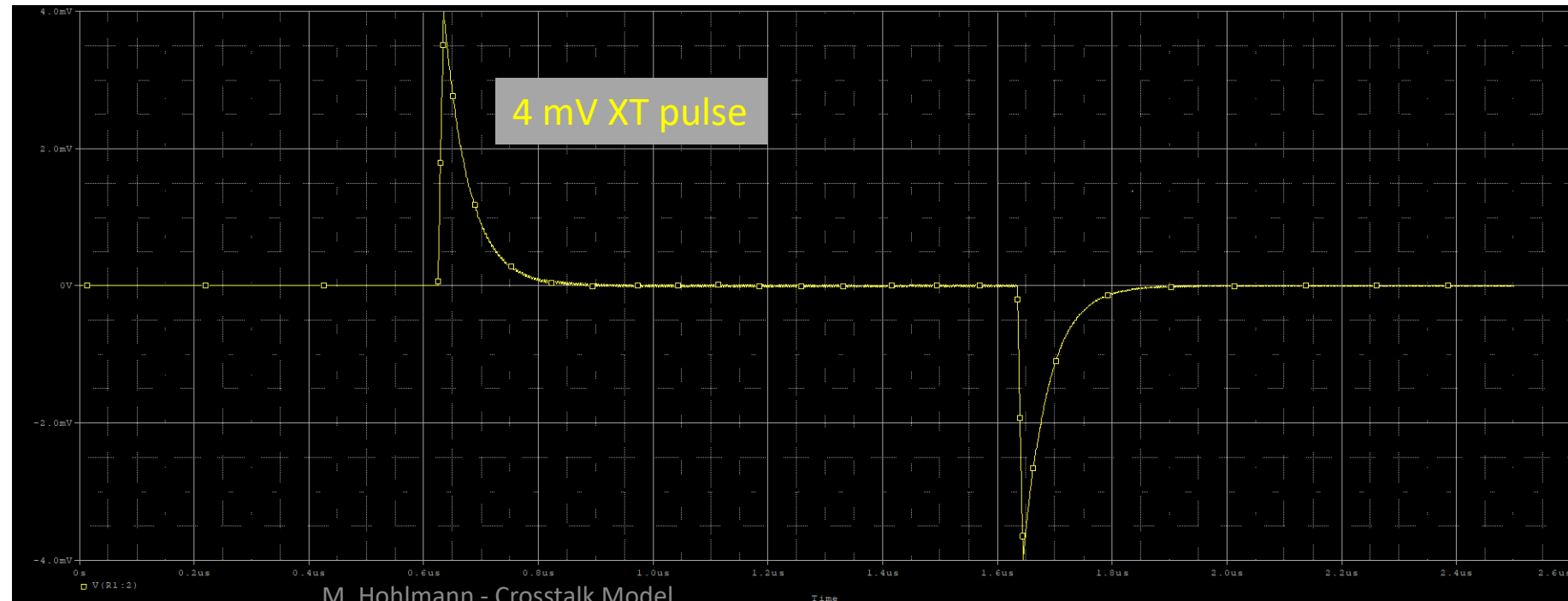
# Tests with Pulsar setup: Limit for bypass capacitor



The problem is again that we still get crosstalk via the direct Interstrip capacitance C6 between signal and XT strip:

Direct short!

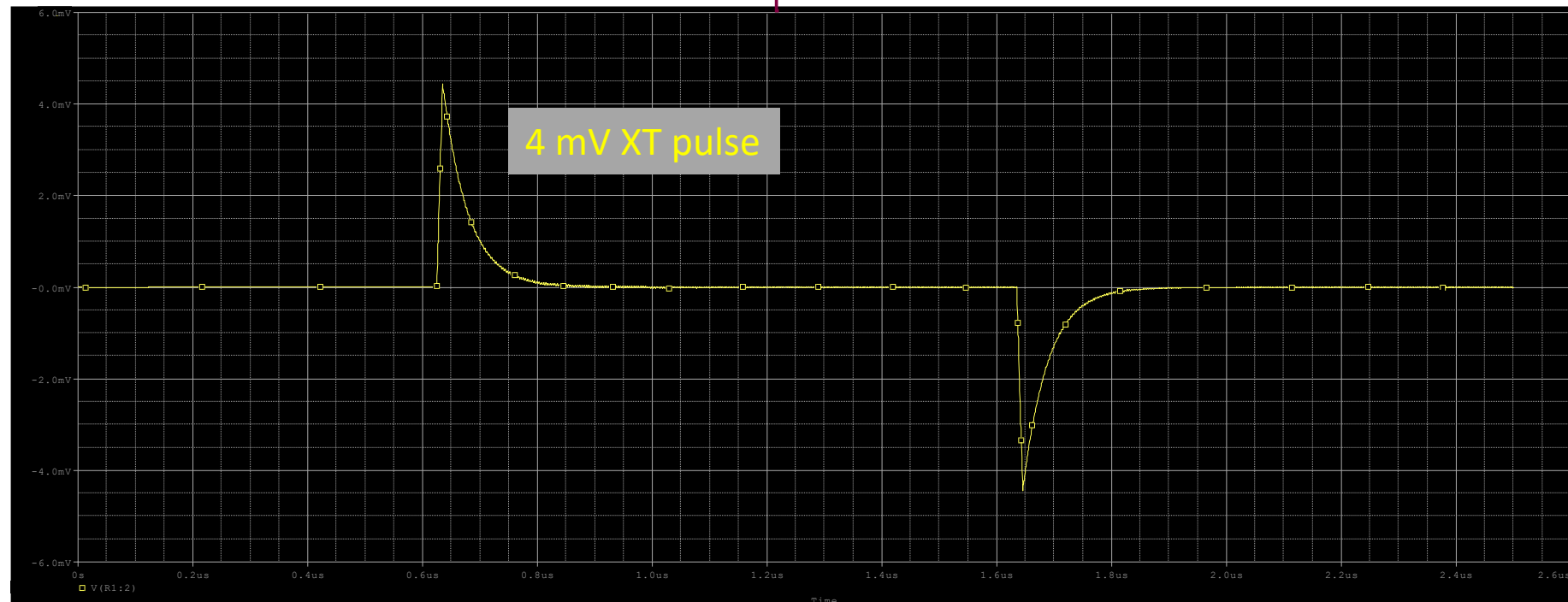
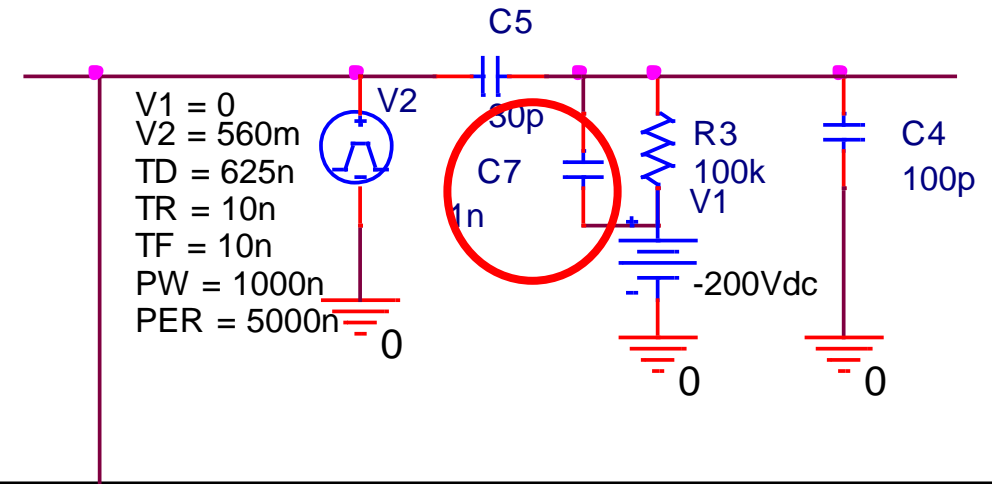
Also  $\approx$  50% reduction of XT  
 (8mV  $\rightarrow$  4 mV)



# Mitigation strategies: Voltage Pulsers Tests

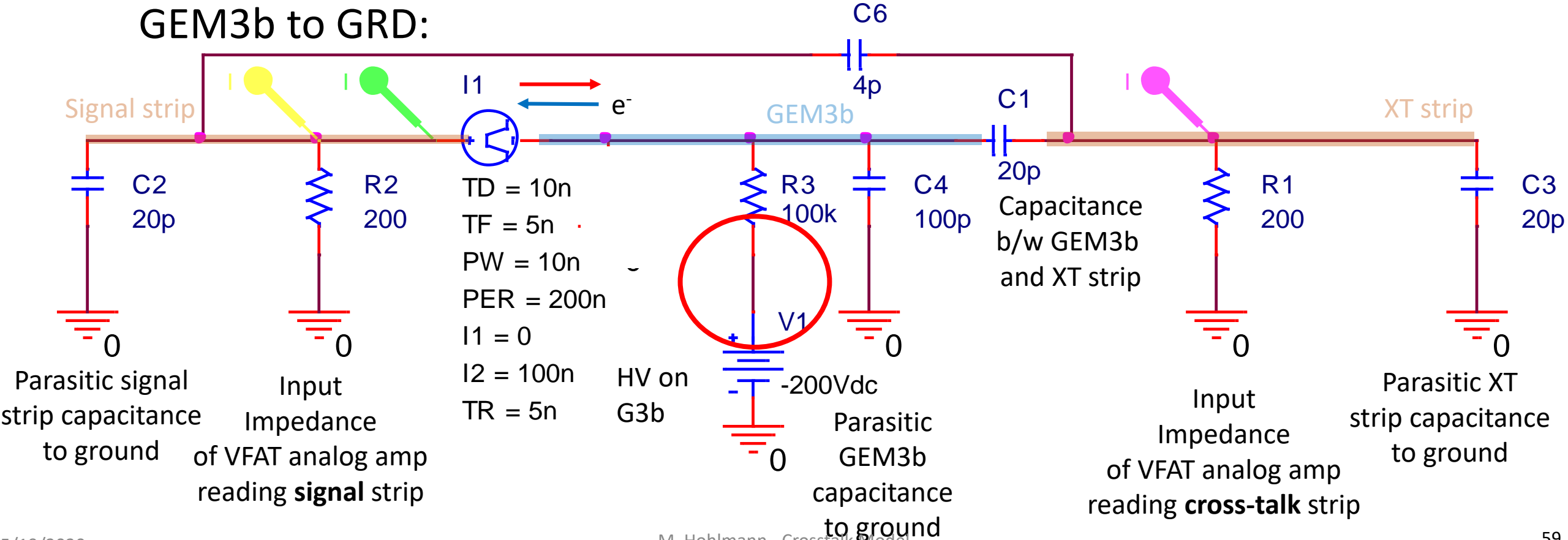
Checking the **impact of bypass (blocking) capacitor on XT with the voltage pulser:**

Expect  $\approx 50\%$  reduction of XT (8mV  $\rightarrow$  4 mV),  
But not as large as factor 4



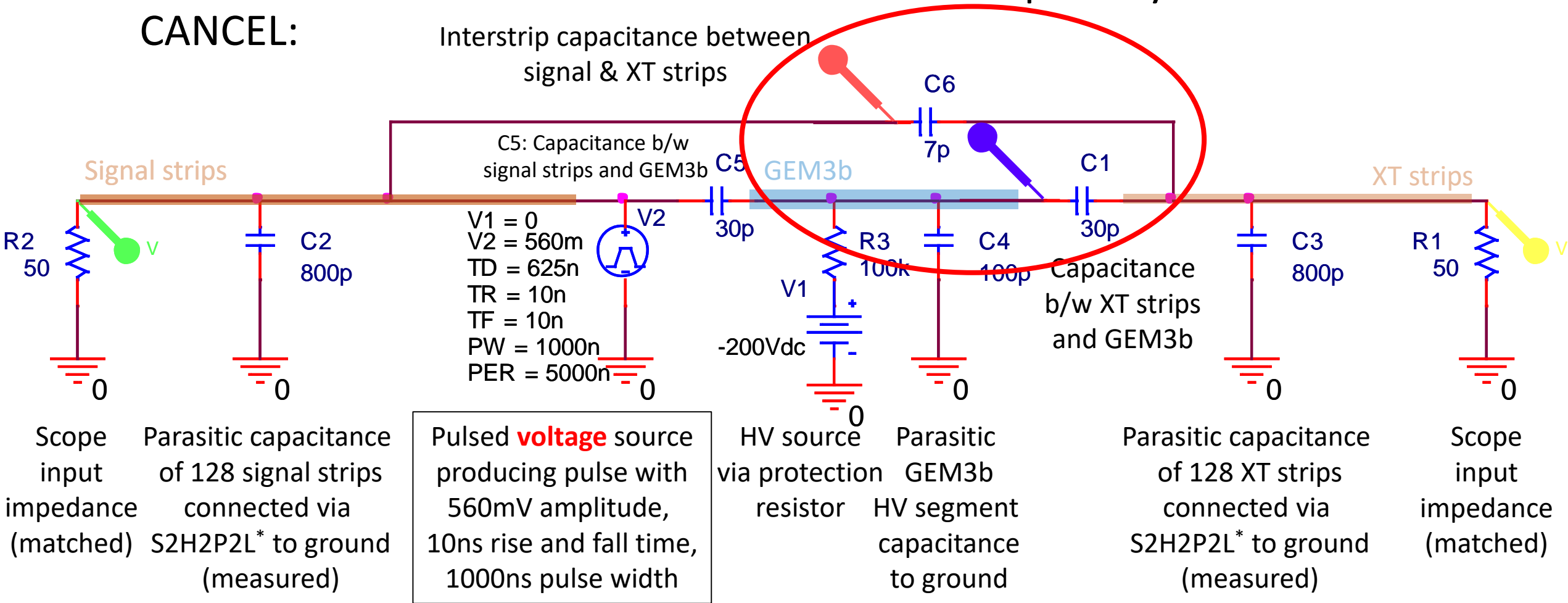
# Mitigation strategies: Other ideas?

- Placing any component **UPSTREAM** of a large protection resistors R3, which would be convenient to do because it could be done with a **single component**, will **NOT** be effective because it will be **in series** with R3 and consequently will **not** reduce the total impedance from GEM3b to GRD:



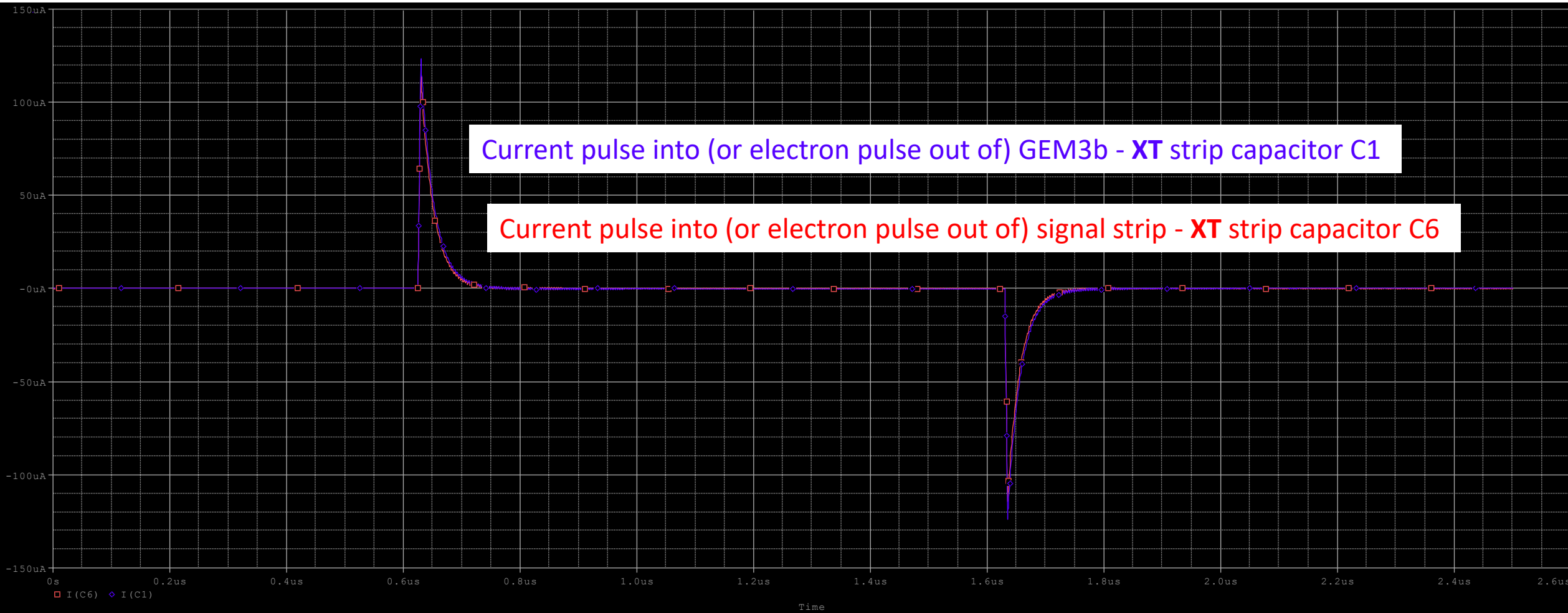
# Mitigation strategies: Overcoming Limitations?

- Unfortunately, we can't test this with the voltage pulser because in this case the two cross-talk currents have the same polarity and do NOT CANCEL:



\* "Strip to Hirose to Panasonic to LEMO" adapter

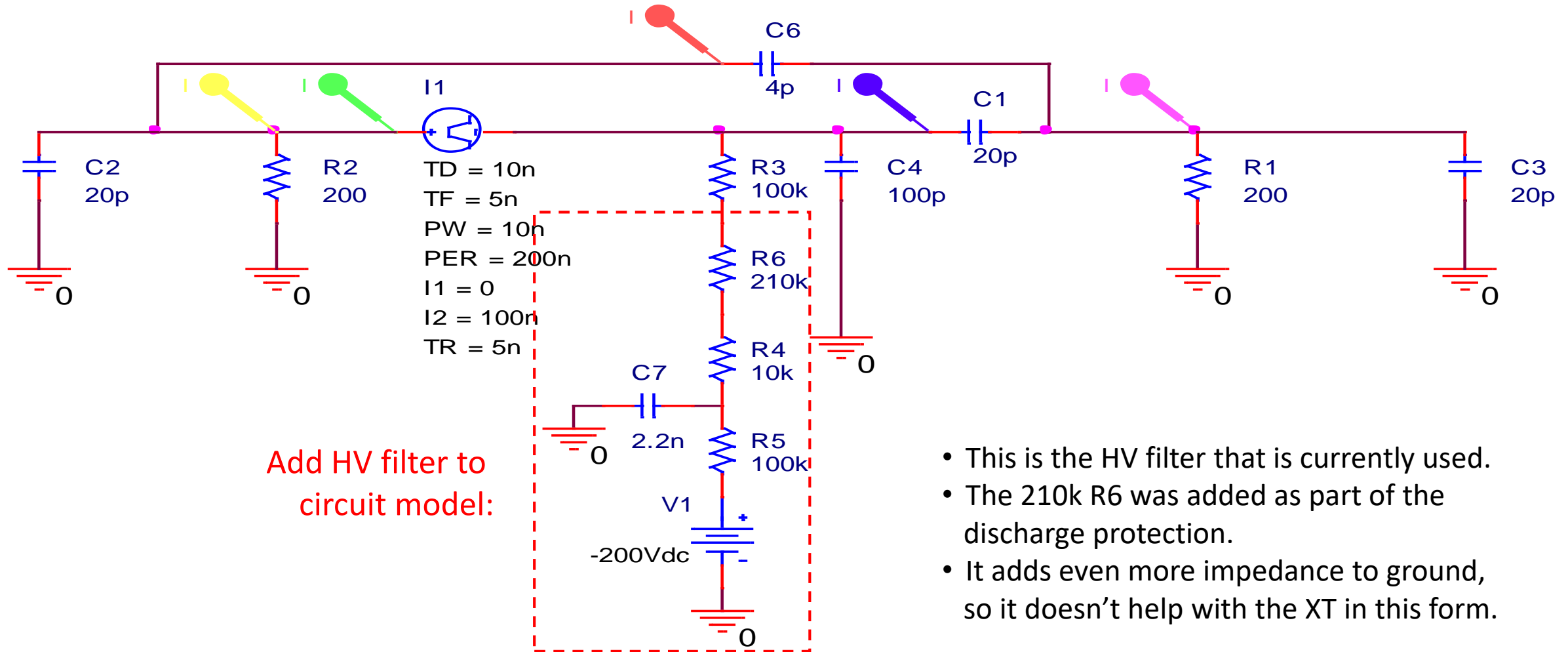
# Mitigation strategies: Overcoming Limitations?



**Main observation:** The two XT contributions have same polarity and do not cancel out. The net XT current is not zero!

# Mitigation strategies: Use HV filter?

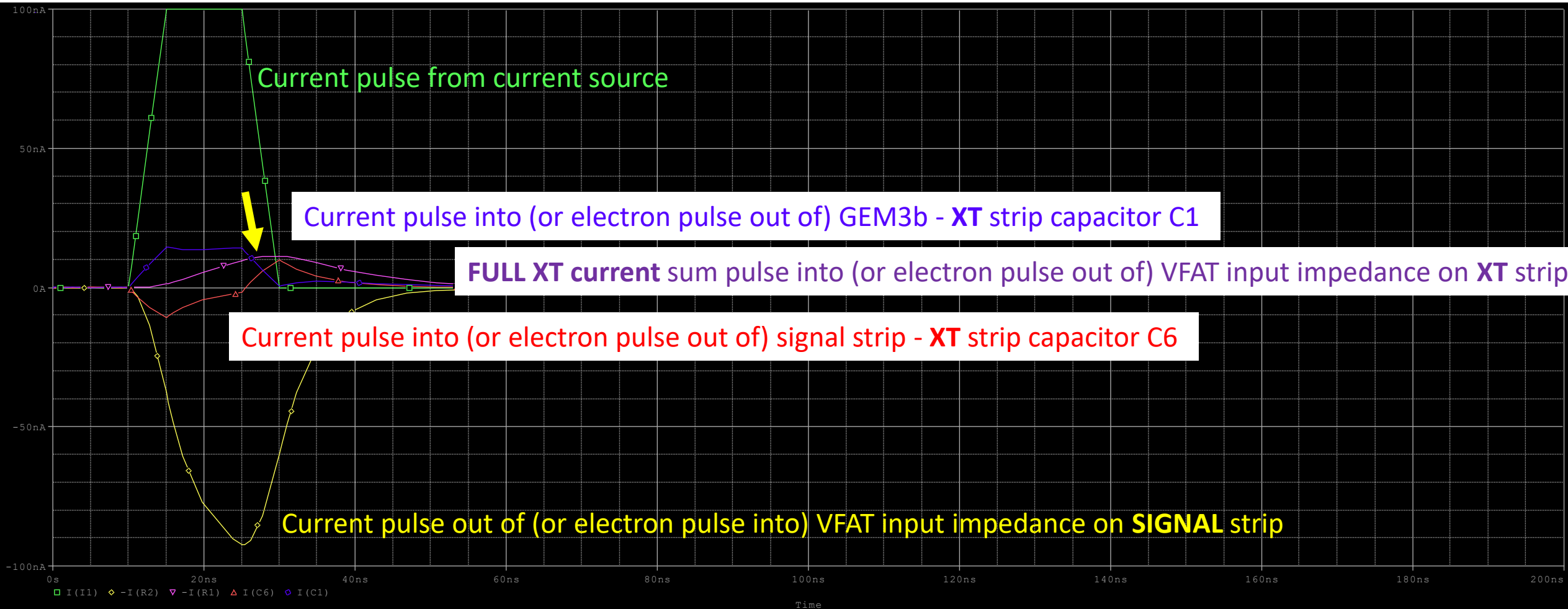
- One example of adding something upstream of R3 is the HV filter:



Add HV filter to circuit model:

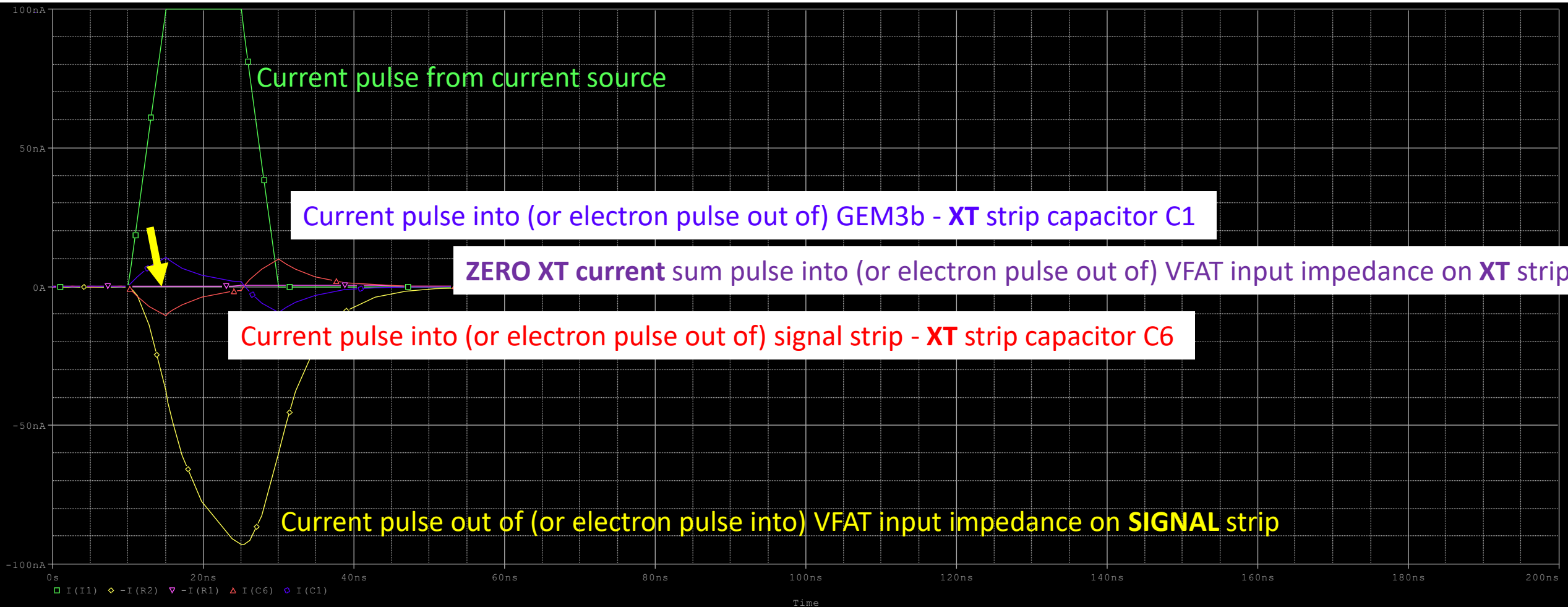
- This is the HV filter that is currently used.
- The 210k R6 was added as part of the discharge protection.
- It adds even more impedance to ground, so it doesn't help with the XT in this form.

# Mitigation strategies: Overcoming Limitations?



**Main observation:** The two XT contributions do not cancel out. The HV filter doesn't help the XT. But at least it doesn't make it worse.

# Mitigation strategies: Overcoming Limitations?



**Main observation:** The two XT contributions have opposite polarity and **cancel out**. The net XT current is zero! The signal current is unaffected.